

## SSLS143 - Pin addition to cantilever with offset heart

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### Summary:

The objective of this test is to validate the calculation of the options `EPSI_ELGA` and `DEGE_ELNO` for the multifibre beams of Euler-Bernoulli `POU_D_EM`, including if the reference axis is not confused with the locus of elastic centres.

The case test also validates the calculation of the elastic matrix ( `RIGI_MECA` ) when the axis of reference is not confused with the locus of elastic centres (offsetting).

## 1 Problem of reference

### 1.1 Geometry

A beam of length  $L=1\text{ m}$  (see Figure 1).

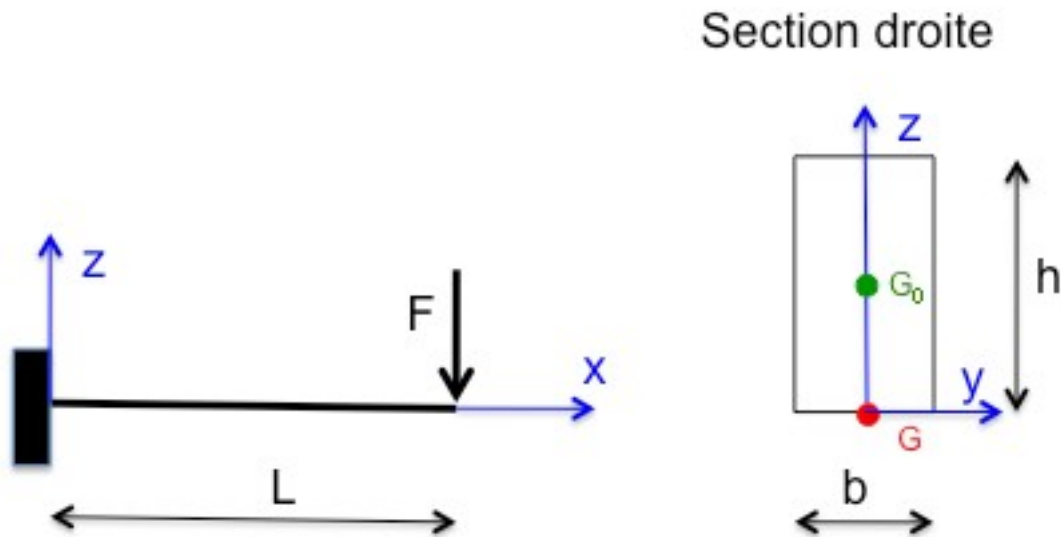


Figure 1: Beam geometry

### 1.2 Properties of material

The cross-section is rectangular  $b \times h = 0.4 \times 1\text{ m}^2$ , and homogeneous with a material of modulus Young  $E = 3 \times 10^{10}\text{ Pa}$ .

### 1.3 Boundary conditions and loadings

The beam is embedded at an end and is charged by a force  $F = 10^6\text{ N}$  at its other end (see Figure 1)

## 2 Reference solution

### 2.1 Analytical expressions

On the basis of the embedded end, the expression of the bending moment is:  $M(x) = F(x-L)$

The arrow at the end charged with the beam is  $f = \frac{FL^3}{EI_{G_0}}$  where  $I_{G_0}$  is the quadratic moment calculated with the barycentre of the section  $G_0$  :  $I_{G_0} = \int_S (y - y_{G_0})^2 dS$ .

Curve in a point located at a distance  $x$  embedding is  $\chi_s(x) = -\frac{M(x)}{EI_{G_0}}$ . Because of the offsetting of the reference axis, the lengthening of the beam (on the level of this axis) is worth:

$\epsilon_s(x) = -\frac{A_G}{S} \chi_s(x)$  where  $S$  is the surface of the section and  $A_G$  static moment of the section compared to an axis passing by  $G$  :  $A_G = \int_S z dS$ .

Deformation of a point of coordinates  $(x, y, z)$  is:  $\epsilon = \epsilon_s(x) - \chi_s(x)z$ , and the constraint at the same point is worth:  $\sigma = E \epsilon$

### 2.2 Calculation of the characteristics of the cross-section

In order to eliminate uncertainty from the approximate digital calculation of the characteristics geometrical of cross-section (low number of fibres), the values used in the reference solution are calculated as in digital calculation:

$$S = \sum_{fibres} S_i \quad A_G = \sum_{fibres} z_i S_i \quad I_G = \sum_{fibres} z_i^2 S_i \quad I_{G_0} = \sum_{fibres} (z_i - z_{G_0})^2 S_i$$

where  $z_i$  is the ordinate of the center of fibre  $i$  and  $S_i$  the surface of this fibre.

## 3 Modeling A

### 3.1 Characteristics of modeling

A modeling is used `POU_D_EM`.

the beam is modelled with 1 finite element and the section is discretized with 8 fibres. The reference axis east chooses voluntarily different from the barycentre, excentré of  $h/2$  to the bottom, with the keyword `COOR_AXE_POUTRE` of `DEFI_GEOM_FIBRE`.

The section "is cut out" in 8 fibres (Figure 2). The coordinates of the centers of fibres and their surfaces are given in table 1.

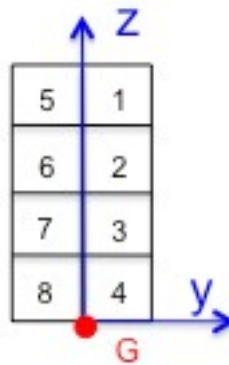


Figure 2: Section division in 8 fibres

Fibres	$y_i$	$z_i$	$S_i$	Fibres	$y_i$	$z_i$	$S_i$
1	0.1	0,875	0.05	5	-0.1	0,875	0.05
2	0.1	0,625	0.05	6	-0.1	0,625	0.05
3	0.1	0,375	0.05	7	-0.1	0,375	0.05
4	0.1	0,125	0.05	8	-0.1	0,125	0.05

Table 1: Characteristics of fibres

### 3.2 Characteristics of the grid

The grid contains 1 elements of the type `SEG2`.

### 3.3 Sizes tested and results

The digital calculation of the sizes of the cross-section gives:

$$S=0.4\text{ m}^2 \quad A_G=0.2\text{ m}^3 \quad I_G=0.13125\text{ m}^4 \quad \text{and} \quad I_{G_0}=0.03125\text{ m}^4$$

The arrow at the end charged with the beam is:  $f=0.00035555\text{ m}$

On the level of embedding  $x=0$  one has the following values:

$$M=-10^{-6}\text{ Nm} \quad \chi_s=0.00106666\text{ m}^{-1} \quad \epsilon_s=-0.00053333\text{ m}^{-1}$$

On the level of the first point of Gauss  $x=(1-\frac{1}{\sqrt{3}})/2=0.21132486540518503\text{ m}$  one has the following values:  $M=-788675.13\text{ Nm} \quad \chi_s=0.00084125\text{ m}^{-1} \quad \epsilon_s=-0.0004206\text{ m}^{-1}$

for the fibre n°1 ( $z=0.875\text{ m}$ ):  $\epsilon=0.00031547$  and  $\sigma=9464101.6\text{ Pa}$  and for the fibre n°4 with  $z=0.125\text{ m}$   $\epsilon=-0.00031547$  and  $\sigma=-9464101.6\text{ Pa}$

Arrow at the end of the beam (DEPL):

Not	Component	Value of reference	Tolerance
SUPPORT	DZ	-3.55555555555555E-4	1.E-6

Deformations generalized with embedding (DEGE\_ELNO):

Mesh	Node	Component	Value of reference	Tolerance
M1	N1	KY	1.066666666666667E-3	1.E-6
M1	N1	EPXX	-5.33333333333333E-3	1.E-6

Strains and stresses in fibres (EPSI\_ELGA and SIEF\_ELGA):

Mesh	Not	Under-point	Component	Value of reference	Tolerance
M1	1	1	EPXX	3.15470053837926E-4	1.E-6
M1	1	1	SIXX	9.46410161513778E6	1.E-6
M1	1	4	EPXX	-3.15470053837926E-4	1.E-6
M1	1	4	SIXX	-9.46410161513778E6	1.E-6

## 4 Summary of the results

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Subject coarsely using the approximate characteristics of the cross-section with a grid for the calculation of the analytical values of reference, the arrow, the constraints and the deformations numerically calculated are identical to these values of reference.