

## ZZZZ330 – Validation of the calculation of the potential energy for the elements of beams

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### Summary:

The objective of this test is to validate the calculation of the potential energy for the elements beams following: POU\_D\_EM , POU\_D\_TG and POU\_D\_TGM.

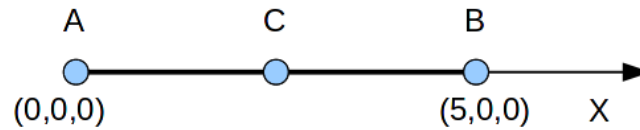
Potential energy is calculated after a static calculation and a modal calculation.

### Note:

| *The validation is already made in addition for the elements POU\_D\_E , POU\_D\_T and POU\_C\_T .*

## 1 Description

### 1.1 Geometry



The model is a beam length  $5\text{ m}$  directed according to the axis  $X$ . This beam consists of 2 meshes SEG2. The section of the beam is rectangular  $HY=0,1\text{ m}$ ,  $HZ=0,2\text{ m}$ .

### 1.2 Properties of materials

The properties of materials are indexed in the following table.

Material	Concrete
Young modulus	$2 \times 10^{10} \text{ Pa}$
Poisson's ratio	0.25
Density	$9167.0 \text{ kg/m}^3$

### 1.3 Boundary conditions and change

The node  $A$  is embedded and the node  $B$  is subjected to a nodal force according to  $Z$  of  $1\text{E}+4 \text{ N}$ .

## 2 Reference solution

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### 2.1 Method of calculating

**In the linear static case:**

$$E_{pot} = W^{ext} = \frac{1}{2} \sum_{i \in N} D_i F_i^{ext} \text{ where } N \text{ is the whole of the nodes of the model.}$$

For a small size it is thus easy to calculate the potential energy starting from displacements.

**In the case of modal calculation:**

If  $\Phi$  is a clean mode of the problem, Eigen frequency  $f = \frac{\omega}{2\pi}$ , with  $K$  matrix of rigidity of  $M$  matrix of mass then  $(K - \omega^2 M)\Phi = 0$ , from where  $\Phi^T (K - \omega^2 M)\Phi = 0$ .  
If one normalizes the modes compared to the matrix of mass  $M$  then one has  $\Phi^T K \Phi = \omega^2 = (2\pi f)^2$ .

However  $E_{pot} = \frac{1}{2} \Phi^T K \Phi$ . It is thus enough to check that  $E_{pot} = 2(\pi f)^2$ .

### 2.2 Sizes and results of reference

### 2.3 Uncertainties on the solution

None.

## 3 Modeling A

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### 3.1 Characteristics of modeling

A modeling is used POU\_D\_EM .

### 3.2 Characteristics of the grid

The grid contains 2 elements of the type SEG2.

### 3.3 Sizes tested and results

#### Static calculation:

The value of the component DZ on the node N3 is tested in nonregression.

Field	Component	Value of reference	Tolerance
EPOT_ELEM	TOTAL	229.9766956	1.E-6

#### Modal calculation:

The value of frequency 7 is tested in nonregression.

Field	Component	Value of reference	Tolerance
EPOT_ELEM	TOTAL	88081.5605639	1.E-6

## 4 Modeling B

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### 4.1 Characteristics of modeling

A modeling is used POU\_D\_TG .

### 4.2 Characteristics of the grid

The grid contains 2 elements of the type SEG2.

### 4.3 Sizes tested and results

#### Static calculation:

The value of the component DZ on the node N3 is tested in nonregression.

Field	Component	Value of reference	Tolerance
EPOT_ELEM	TOTAL	226.34657911364	1.E-6

#### Modal calculation:

The value of frequency 7 is tested in nonregression.

Field	Component	Value of reference	Tolerance
EPOT_ELEM	TOTAL	96160.162695954	1.E-6

## 5 Modeling C

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### 5.1 Characteristics of modeling

A modeling is used POU\_D\_ TGM.

### 5.2 Characteristics of the grid

The grid contains 2 elements of the type SEG2.

### 5.3 Sizes tested and results

#### Static calculation:

The value of the component DZ on the node N3 is tested in nonregression.

Field	Component	Value of reference	Tolerance
EPOT_ELEM	TOTAL	230.67091447835	1.E-6

#### Modal calculation:

The value of frequency 7 is tested in nonregression.

Field	Component	Value of reference	Tolerance
EPOT_ELEM	TOTAL	94759.34489198	1.E-6

## 6 Summary of the results

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The values of reference for the potential energy are found in each modeling for the two different types of calculation.