

TTLP303 - Transfer of heat in an orthotropic plate: imposed temperatures

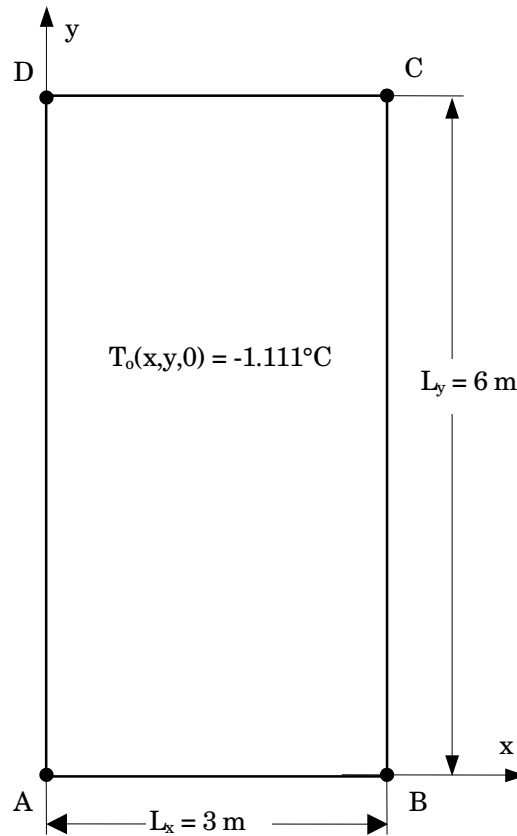
Summary:

This test is resulting from the validation independent of version 3 in thermics.

| | |
|-----------------------|---|
| Analysis: | Linear transitory thermics |
| Problem: | 2D plan |
| Features tested: | <ul style="list-style-type: none">• thermal element hull• thermal element plan• orthotropic material• transitory algorithm of thermics• limiting conditions: imposed temperatures |
| Interest of the test: | <ul style="list-style-type: none">• orthotropic material• analytical solution |
| Many modelings: | <ul style="list-style-type: none">• 1 modeling hull• 1 plane modeling |

1 Problem of reference

1.1 Geometry



1.2 Properties of material

| | |
|---|---|
| $\lambda_x = 1.319 \text{ W/m}^\circ\text{C}$ | thermal conductivity along the axis x |
| $\lambda_y = 0.659 \text{ W/m}^\circ\text{C}$ | thermal conductivity along the axis y |
| $\rho C = 1899.1 \text{ J/m}^3^\circ\text{C}$ | voluminal heat |

1.3 Boundary conditions and loadings

Contour $ABCD$: $T = -17.778^\circ\text{C}$

1.4 Initial conditions

$$T_0(t=0) = -1.111^\circ\text{C}$$

2 Reference solution

2.1 Method of calculating used for the reference solution

$$T(x, y, t) = \sum_{n=1}^{\infty} \sum_{j=1}^{\infty} A_n \sin \frac{n\pi x}{L_x} \sin \frac{j\pi y}{L_y} \exp \left[- \left(\frac{\lambda_x n^2 \pi^2}{L_x^2} + \frac{\lambda_y j^2 \pi^2}{L_y^2} \right) t / \rho c \right]$$

where $A_n = \left[\frac{4(T_i)}{\pi^2 j n} [(-1)^n - 1][(-1)^j - 1] - 32 \right] \frac{5}{9}$ $T_i = \frac{5}{9} T_0 + 32$

Temperature in °C with $t = 4320s$

| | | | | | | |
|-----|----------|----------|----------|----------|----------|----------|
| 3.0 | -17.7778 | -17.5742 | -17.3905 | -17.2448 | -17.1515 | -17.1189 |
| 2.7 | -17.7778 | -17.5764 | -17.3948 | -17.2507 | -17.1581 | -17.1262 |
| 2.4 | -17.7778 | -17.5832 | -17.4077 | -17.2684 | -17.1790 | -17.1482 |
| 2.1 | -17.7778 | -17.5945 | -17.4291 | -17.2979 | -17.2137 | -17.1847 |
| 1.8 | -17.7778 | -17.6102 | -17.4590 | -17.3391 | -17.2620 | -17.2355 |
| 1.5 | -17.7778 | -17.6302 | -17.4970 | -17.3914 | -17.3235 | -17.3002 |
| 1.2 | -17.7778 | -17.6542 | -17.5426 | -17.4541 | -17.3973 | -17.3777 |
| 0.9 | -17.7778 | -17.6816 | -17.5949 | -17.5261 | -17.4819 | -17.4667 |
| 0.6 | -17.7778 | -17.7120 | -17.6526 | -17.6056 | -17.5753 | -17.5649 |
| 0.3 | -17.7778 | -17.7444 | -17.7142 | -17.6903 | -17.6749 | -17.6696 |
| 0.0 | -17.7778 | -17.7778 | -17.7778 | -17.7778 | -17.7778 | -17.7778 |

Y ↑
X → 0.0 0.3 0.6 0.9 1.2 1.5

The values of reference are obtained with $n = j = 1000$

2.2 Results of reference

$t = 4320s (1.2hr)$: temperature at the following points:

- in $x = 0.6$: for $y = 0.6, 1.5, 2.4, 3.0$
- in $x = 1.5$: for $y = 0.6, 1.5, 2.4, 3.0$

2.3 Uncertainty on the solution

Analytical solution.

2.4 Bibliographical references

1. J.C. Bruch Jr., G. Zyrolowski, 'Transient two-dimensional heat conduction problems solved by the finite element method', Int. J. num. Meth. Engng, flight 8, n°3, pp 481-494, 1974.

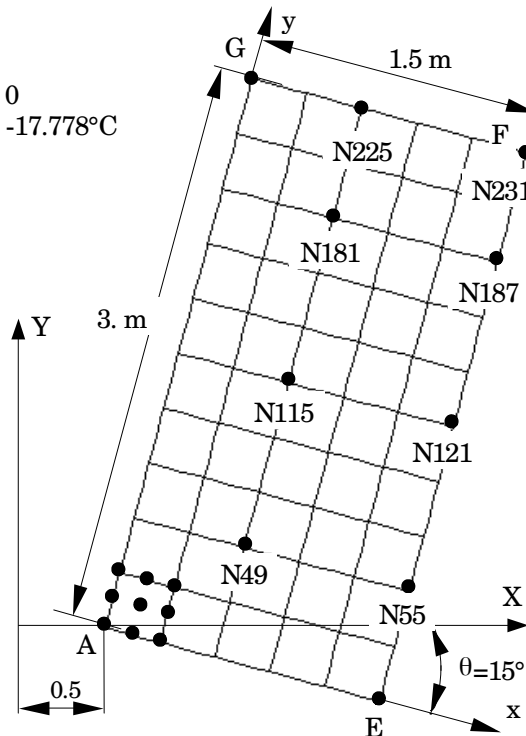
3 Modeling C

3.1 Characteristics of modeling

PLAN (QUAD9)

Conditions limites

- cotés EF, FG: $\phi = 0$
- cotés AE, AG: $T = -17.778^{\circ}\text{C}$



3.2 Characteristics of the grid

Many nodes: 231
Many meshes and types: 50 QUAD9

3.3 Remarks

The discretization in step of time is the following one:

240 pas for $[0., 4320.D0]$ that is to say $\Delta t = 18.D0$

4 Results of modeling C

4.1 Values tested

| Identification | Reference | Aster | Relative variation % | | Absolute deviation | |
|-------------------------------|-----------|----------|----------------------|-----------|--------------------|-----------|
| | | | difference | tolerance | difference | tolerance |
| Temperature in °C | | | | | | |
| <i>x</i> = 0.6 | | | | | | |
| <i>N49</i> (<i>y</i> = 0.6) | -17.6526 | -17.6515 | -0,006 | 1% | 0,001 | 0.05 |
| <i>N115</i> (<i>y</i> = 1.5) | -17.4970 | -17.4942 | -0,016 | 1% | 0,003 | 0.05 |
| <i>N181</i> (<i>y</i> = 2.4) | -17.4077 | -17.4040 | -0,021 | 1% | 0,004 | 0.05 |
| <i>N225</i> (<i>y</i> = 3.0) | -17.3905 | -17.3867 | -0,022 | 1% | 0,004 | 0.05 |
| <i>x</i> = 1.5 | | | | | | |
| <i>T</i> (<i>y</i> = 0.6) | -17.5649 | -17.5627 | -0,012 | 1% | 0,002 | 0.05 |
| <i>T</i> (<i>y</i> = 1.5) | -17.3002 | -17.2952 | -0,029 | 1% | 0,005 | 0.05 |
| <i>T</i> (<i>y</i> = 2.4) | -17.1482 | -17.1418 | -0,037 | 1% | 0,006 | 0.06 |
| <i>T</i> (<i>y</i> = 3.0) | -17.1189 | -17.1123 | -0,039 | 1% | 0,007 | 0.05 |

5 Summary of the results

Modeling PLAN, carried out with meshes QUAD9, gives satisfactory results, the maximum change obtained is of 0,039%.