

## SZLZ101 - Computation of the damage/Method RAINFLOW

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### Summarized:

The purpose of this test is computation of the damage from a load history in stresses.

From a simple load history defined by `DEFI_FONCTION`, one extracts the elementary cycles by the method of counting of cycles of the RAINFLOW [R7.04.01], then one calculates the elementary damage associated with each cycle, by interpolation on the curve of Wöhler of the material.

One tests various possibilities of introducing the curve of Wöhler, as well as the taking into account of the elastoplastic coefficient of concentration.

To finish, one determines the total damage undergone by the part by cumulating all the elementary damages by the linear rule To mine.

This example is a test of validation of software POSTDAM developed by Department REME, provided in the handbook of validation of version 1.0 of this software.

Results provided by the operator `POST_FATIGUE` are completely identical to those provided by software POSTDAM.

## 1 Problem of reference

### 1.1 Geometry

the analysis consists in determining the damage undergone by a part in a point to which one provides the load history in stresses.

From a simple load history defined by `DEFI_FONCTION`, one extracts the elementary cycles by the method of counting of cycles of RAINFLOW [R7.04.01], then one calculates the elementary damage associated with each cycle, by interpolation on the curve of Wöhler of the material.

One tests various possibilities of introducing the curve of Wöhler and the taking into account or not of an elastoplastic coefficient of concentration:

- The curve of Wöhler is defined in the form:

$$S_{alt} = \text{contrainte alternée} = 1/2(E_c/E)\Delta\sigma \quad X = \text{LOG}_{10}(S_{alt})$$

$$N = 10^{a0 + a1X + a2X^2 + a3X^3} \quad D = \begin{cases} 1/N & \text{si } S_{alt} \geq S_l \\ 0 & \text{sinon} \end{cases}$$

with:

$E_c$  = Young Modulus associated with the curve with fatigue with the material,

$E$  = Young Modulus used to determine the stresses,

constants of the material  $a0$   $a1$ ,  $a2$  and  $a3$ ,

and  $S_l$  limit of endurance of the material.

- The curve of Wöhler is defined in the same form and moreover one takes account of an elastoplastic coefficient of concentration defined by:

$$\begin{cases} K_e = 1 & \text{si } \Delta\sigma < 3S_m \\ K_e = 1 + (1-n)/(\Delta\sigma/3S_m - 1)/(n(m-1)) & \text{si } 3S_m < \Delta\sigma < 3mS_m \\ K_e = 1/n & \text{si } 3mS_m < \Delta\sigma \end{cases}$$

where

$S_m$  is the acceptable maximum stress,

and  $n$   $m$  two constants depending on the material.

- The curve of Wöhler is defined in the analytical form of Basquin:  $D = A S_{alt}^\beta$

To finish, one determines the total damage undergone by the part by cumulating all the elementary damages by the linear rule To mine.

### 1.2 Material properties

Parameters of definition of the curve of Wöhler:

$a0$	$a1$	$a2$	$a3$	$Ec$	$E$	$Sl$
55.81	-43.06	11.91	-1.16	200000.	200000.	180.

Parameters of definition of the elastoplastic coefficient of concentration  $K_e$  :

$Sm$	$n$	$m$
126.	0.3.1.7	

Parameters of definition of the curve of Wöhler in the form analytical of Basquin:

$A$	$\beta$
1.001730939 E-14	4.065

**History of the loading**

$t$	0.	1.	2.

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$\sigma(t)$       0.      1000.      0.

## 2 Reference solution

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### 2.1 Method of calculating used for the reference solution

This test is resulting from the handbook of validation of software POSTDAM version 1.0. The reference solutions are given in this document.

### 2.2 Results of reference

the counting of the elementary cycles by method RAINFLOW leads to:

Nb\_Cycl = 1      Cycle 1      Vale\_Min:      0.      Vale\_Max:      1000.

- **First call** to POST\_FATIGUE :

                 Cycle 1      Damage:      2.858503E-4

                 The computation of the total damage by linear office plurality To mine:

                 Too bad: 2.858503E-4

- **Second call** to POST\_FATIGUE :

                 Cycle 1      Damage:      1.224941E-2

                 The computation of the total damage by linear office plurality To mine:

                 Too bad: 1.224941E-2

- **Third call** to POST\_FATIGUE :

                 Cycle 1      Damage:      9.377005E-4

                 The computation of the total damage by linear office plurality To mine:

                 Too bad: 9.377005E-4

### 2.3 Uncertainty on the analytical

solution Solution.

### 2.4 Bibliographical references

1. Handbook of validation POSTDAM 1.0. Baker I., Vatin E. HP-14/93/016/B.

## 3 Modelization A

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### 3.1 Quantities tested and results

Identification		Reference
NB_CYCL		1.
Cycle 1	VALE_MIN	0.
	VALE_MAX	1000.
<b>First call to POST_FATIGUE :</b>		
Cycle 1	DOMMAGE	2.858503E-4
	DOMM_CUMU	2.858503E-4
<b>Second call to POST_FATIGUE :</b>		
Cycle 1	DOMMAGE	1.22494E-2
	DOMM_CUMU	1.22494E-2
<b>Third call to POST_FATIGUE :</b>		
Cycle 1	DOMMAGE	9.377005E-4
	DOMM_CUMU	9.377005E-4

## 4 Summary of the results

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the results provided by Code\_Aster are perfectly identical to the values of reference.