

## HSNV133 - Thermoplastic tension in large deformations VMIS ISOT PUIS

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### Summarized:

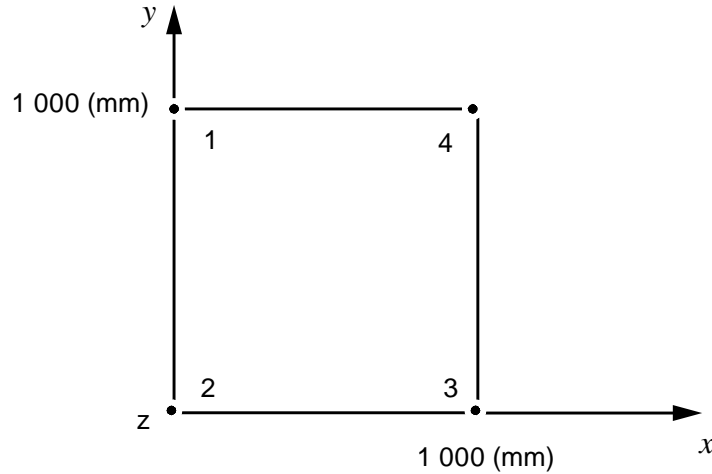
This quasi-static thermomechanical test consists in uniformly heating a bar of rectangular section (stress states and homogeneous strains) then to subject it to a tension.

In the same way, that in test HSNV121 [V7.22.121], one thus validates the kinematics of the large deformations in elastoplasticity (command `STAT_NON_LINE`, key word strain: "SIMO\_MIEHE" or "PETIT\_REAC") for a behavior model of the type Von Mises with definite isotropic hardening is by a point by point given curve of tension (VMIS\_ISOT\_TRAC); maybe by a model in power (VMIS\_ISOT\_PUIS).

The bar is modelled by a voluminal element (HEXA20, modelization A).

## 1 Problem of reference

### 1.1 Geometry



### 1.2 Properties of the material

the material obeys a constitutive law in plastic large deformations with isotropic hardening defined by a curve of tension (point by point or model in power).

Curve of tension is given in the logarithmic strain plane - rational stress.

$$\sigma = \frac{F}{S} = \frac{F}{S_o} \cdot \frac{l}{l_o}$$

$$R(p) = \sigma_y + \sigma_y \left( \frac{E}{a \sigma_y} p \right)^{1/n}$$

$$\nu = 0.3$$

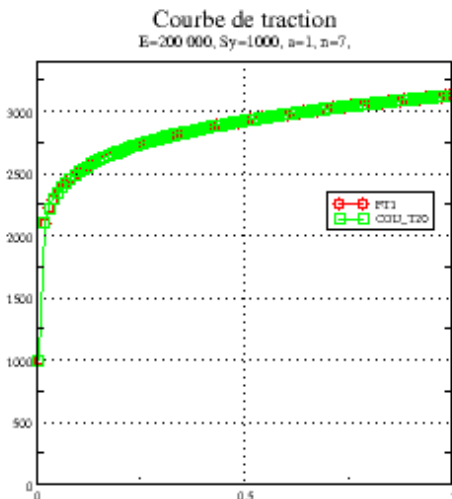
$$\alpha = 10^{-4} K^{-1}$$

$$\sigma_y = 1000 \text{ MPa}$$

$$E = 200000 \text{ MPa}$$

$$n = 7$$

$$a = 1$$

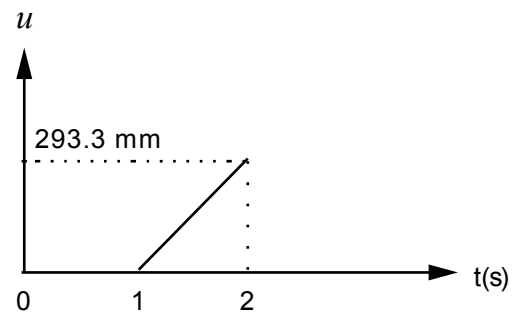
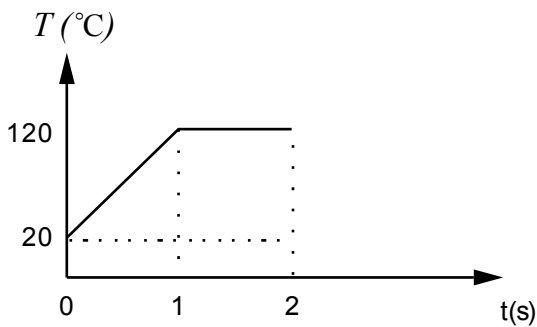
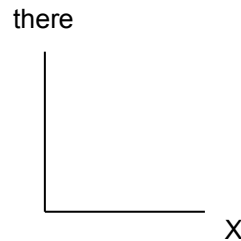
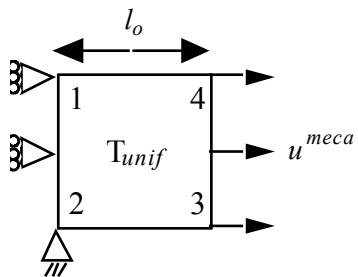


$l_o$  and  $l$  are, respectively, the initial length and the current length of the useful part of the test-tube.

$S_o$  and  $S$  are, respectively, surfaces initial and current. Between the temperatures  $20^\circ C$  and  $120^\circ C$ , the characteristics are interpolated linearly.

## 1.3 Boundary conditions and loadings

the bar, initial length  $l_o$ , blocked in the direction  $Ox$  on the face [1,2] is subjected to a uniform temperature  $T$  and a mechanical displacement of tension  $u^{meca}$  on the face [3, 4]. The sequences of loading are the following ones:



Reference temperature:  $T_{réf} = 20^\circ C$ .

**Note:**

*Mechanical displacement is measured from the configuration deformed by the thermal loading ( $t=1$ s). To have total displacement, it is thus necessary to add the thermal displacement obtained at time  $t=1$ s.*

## 2 Reference solution

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### 2.1 Results of reference

One will adopt like results of reference displacements, the stress of Cauchy  $\sigma$  and the cumulated plastic strain  $p$  obtained with behavior VMIS\_ISOT\_TRAC (validated in addition with DEFORMATION=' SIMO\_MIEHE ').

One will compare the solutions obtained with time  $t=2\text{ s}$  ( $\Delta T = 100^\circ\text{C}$ , tension  $u$ )

### 2.2 Uncertainty on the Very

weak solution since it is about intercomparison between two behaviors formally identical. However, the discretization of the model of hardening in power leads to an uncertainty.

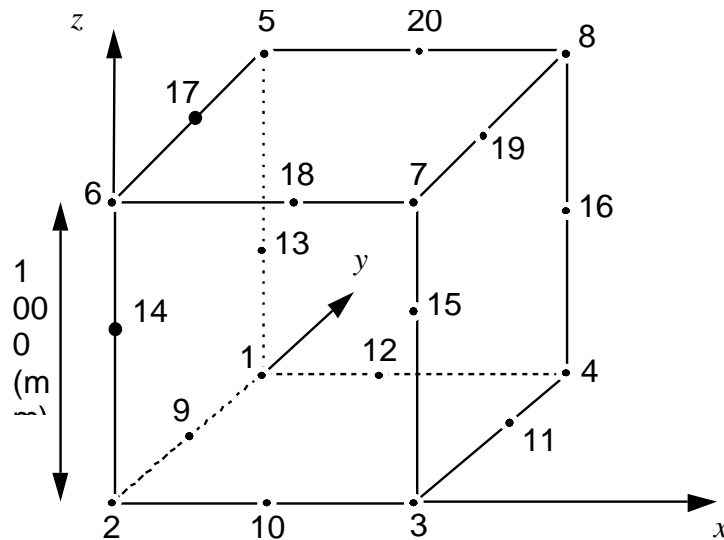
### 2.3 Bibliographical references

- 1.V. CANO, E. LORENTZ: Introduction into *the Code\_Aster* of an elastoplastic model of behavior in large deformations with isotropic hardening - internal Note EDF DER HI - 74/98/006/0

## 3 Modelization A

### 3.1 Characteristic of the voluminal

modelization Modelization: 1 mesh HEXA20  
1 nets QUAD8



**Boundary conditions:**

$$\begin{aligned} \text{N2:} \quad & U_x = U_y = U_z = 0 & \text{N9, N13, N14, N5, N17 : } & U_x = 0 \\ \text{N1:} \quad & U_x = U_z = 0 \\ \text{N6:} \quad & U_x = U_y = 0 \end{aligned}$$

**Charge:** Displacement imposed on the face [348711161915] + assignment of the same temperature on all the nodes. The nombre total of increments is of 21 (1 increment enters  $t=0s$  and  $1s$ , 20 increments enters  $t=1s$  and  $2s$ ).

Convergence is carried out if the residue is lower or equal to  $\text{RESI\_GLOB\_RELA} = 10^{-6}$ .

### 3.2 Characteristics of the mesh

Many nodes: 20

Number of meshes: 2

1 HEXA20  
1 QUAD8

### 3.3 Quantities tested and results

Identification	Reference	Aster	% difference
	VMIS_ISOT_TRAC	VMIS_ISOT_PUIS	
$t=2$ Displacement $DX$ (N8)	303.06	303.06	< 10-4
$t=2$ Displacement $DY$ (N8)	- 108.82	- 108.82	< 10-4
$t=2$ Displacement $DZ$ (N8)	- 108.82	- 108.82	< 10-4
$t=2$ Stresses $SIGXX$ (PG1)	2651.633	2651.694	0.002
$t=2$ Variable $p$ $VARI$ (PG1)	0.24556	0.24558	0.009

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## 4 Summary of the results

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inter-validation of behaviors `VMIS_ISOT_TRAC` and `VMIS_ISOT_PUIS` realized here watch that the curves of isotropic hardening can be modelled in these two ways in *Code\_Aster*, that it is into small or large deformations, via the model "SIMO\_MIEHE".