

## SSNV211 - Triaxial compression test drained with the model VISC\_DRUC\_PRAG

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### Summarized

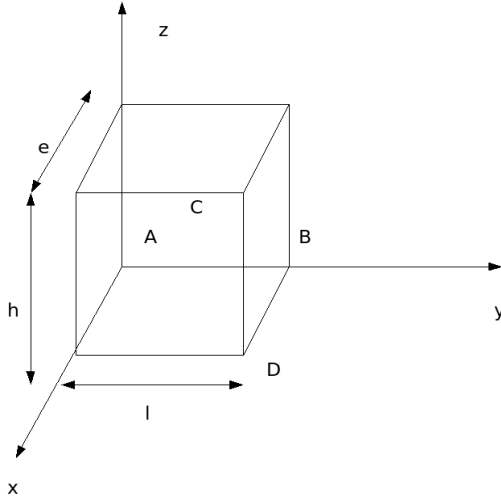
This test makes it possible to validate VISC\_DRUC\_PRAG the model based on the model élastoplastique Drucker-Prager. creep is taken into account by a model power of the Perzyna type. It is about a triaxial compression test in pure mechanics or drained condition. Computations are carried out only on the solid part of the soil without hydraulic coupling. One applies a level of containment of  $5 \text{ MPa}$ . By reason of symmetry, one is interested only in the eighth of a sample subjected to a triaxial compression test. The modelization is axisymmetric.

It is about a test of non regression.

## 1 Problem of reference

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### 1.1 Geometry



height:  $h = 1 \text{ m}$   
width:  $l = 1 \text{ m}$   
thickness:  $e = 1 \text{ m}$

Coordinates of the points (in meters):

	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>
<i>x</i>	0.	0.	0.5	1.
<i>y</i>	0.	1.	0.5	1.
<i>z</i>	0.	0.	0.5	0.

## 1.2 Material property

elastic properties under key word ELAS:

$$E = 5000.0 \text{ in } MPa$$

$$\nu = 0.12$$

$$\alpha = 0.0$$

viscoplastic properties under word VISC\_DRUC\_PRAG:

$$P_{ref} = 0.1 \text{ in } MPa$$

$$A = 1.5 \cdot 10^{-12} \text{ of } s^{-1}$$

$$n = 4.5$$

$$p_{pic} = 0.015$$

$$p_{ult} = 0.028$$

$$\alpha_0 = 0.065$$

$$\alpha_{pic} = 0.26$$

$$\alpha_{ult} = 0.091$$

$$R_0 = 1.3021 \text{ } MPa$$

$$R_{pic} = 6.24808 \text{ of } MPa$$

$$R_{ult} = 1.30808 \text{ } Mpa$$

$$\beta_0 = -0.15$$

$$\beta_{pic} = 0.$$

$$\beta_{ult} = 0.13$$

## 1.3 Initial conditions, boundary conditions, and loading

### Phase 1:

One brings the sample in a homogeneous state:  $\sigma_{xx}^0 = \sigma_{yy}^0 = \sigma_{zz}^0$ , by imposing the corresponding confining pressure on the front, side right and higher sides. Displacements are blocked on the sides postpones ( $u_x = 0$ ), side left ( $u_y = 0$ ) and lower ( $u_z = 0$ ).

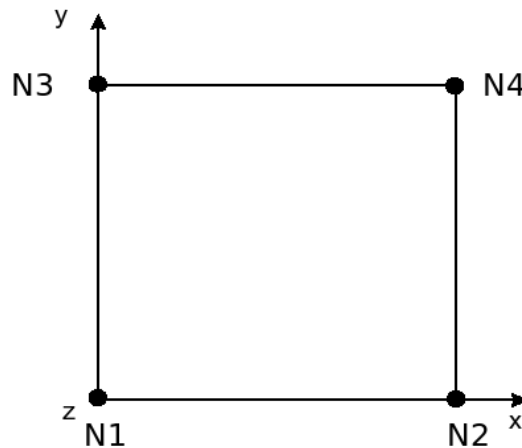
### Phase 2:

One maintains displacements blocked on the sides postpones ( $u_x = 0$ ), side left ( $u_y = 0$ ) and lower ( $u_z = 0$ ), as well as the confining pressure on the front sides and side right. One applies a displacement imposed to the upper face:  $u_z(t)$ , in order to obtain a strain  $\varepsilon_{zz} = -6$ .

## 2 Modelization A

### 2.1 Characteristic of the modelization

2D\_Axi :



Cutting: 1 in height, 1 in width.

Loading of phase 1:

Confining pressure:  $\sigma_{xx}^0 = \sigma_{zz}^0 = -5 \text{ MPa}$

### 2.2 Characteristic of the mesh

Many nodes: 4

Number of meshes and types: 1 QUAD4 and 4 SEG2

### 2.3 Quantities tested and results

For  $\sigma_{xx}^0 = \sigma_{zz}^0 = -5 \text{ MPa}$

Localization	Time	Forced ( MPa )	Aster
Point <i>N4</i>	7000.	$\sigma_{yy}$	- 5.000
	13000.	$\sigma_{yy}$	- 11.667
Localization	Time	Aster	Displacement
Point <i>N4</i>	7000.	<i>DX</i>	-7.6 10-4
	13000.	<i>DX</i>	3.4598 10-2

## 3 Summary of the results

It acts of a test of non regression developed to validate VISC\_DRUC\_PRAG in pure mechanics the model.