

## **SSNV102 - Traction test shears with the model of TAHERI**

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### **Summarized:**

The problem is quasi-static nonlinear in structural mechanics.

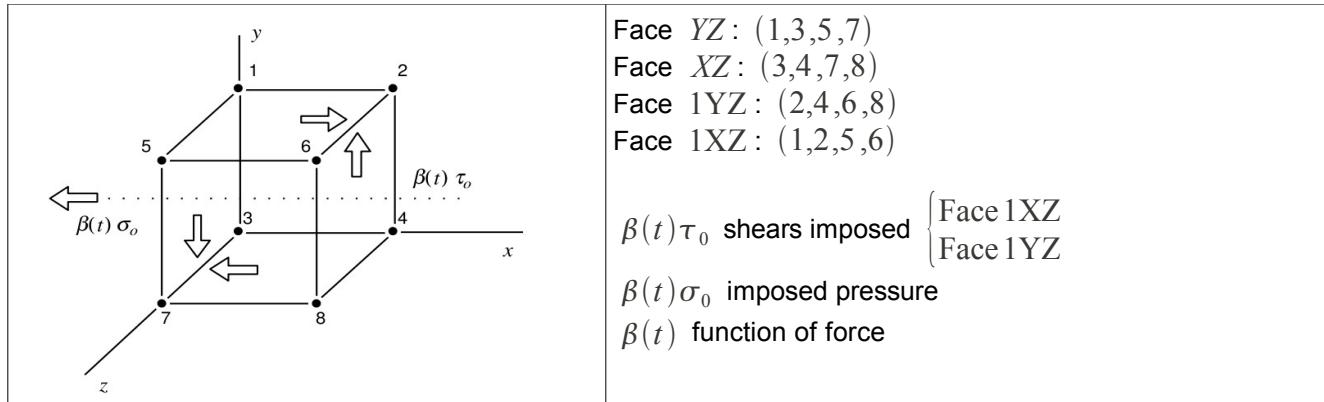
One analyzes the response of a volume element with a loading in tension-shears, carried out in such way that imposes a state of uniform stress-strain in the element.

There are 2 modelizations: one into 3D voluminal and another in plane stresses 2D .

One validates by this test the numerical integration of the elastoplastic model of behavior of Saïd Taheri.

## 1 Problem of reference

### 1.1 Geometry

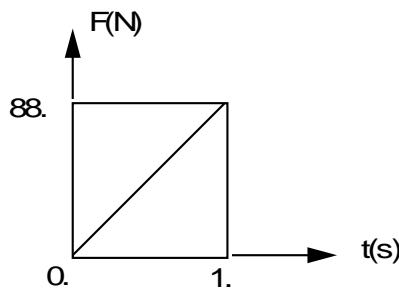


### 1.2 Material properties

isotropic elasticity	$E = 200\,000 \text{ MPa}$	$\nu = 0,3$
plasticity Taheri	$C_{inf} = 0.065 \text{ MPa}$	$C_1 = -0.012 \text{ MPa}$
	$m = 0.1$	$s = 450 \quad b = 30$
		$a = 312 \quad \alpha = 0.3 \quad R_o = 72$

### 1.3 Boundary conditions and loadings

$N04$	$dx = dy = 0$	Face $YZ :$	$FX = FY = -F(t)$
$N08$	$dx = dy = dz = 0$	Face $XZ :$	$FX = -F(t)$
$N02, N06$	$dx = 0$	Face $1YZ :$	$FY = F(t)$
		Face $1XZ :$	$FX = F(t)$



### 1.4 Forced

initial conditions and null strains with  $t = 0$ .

## 2 Reference solution

### 2.1 Method of calculating used for the reference solution

One integrates the following system numerically enters  $t=0$  and  $t=1$ .

(Nonlinear ordinary Differential connection of 6 equations to 6 unknowns solved using library NAG by a "Backward difference method")

$$\dot{\varepsilon} - \dot{\varepsilon}_p = \beta \frac{\sigma_o}{E} \quad \text{éq 2.1-1}$$

$$\dot{\gamma} - \dot{\gamma}_p = \beta \frac{\tau_o}{2\mu} \quad \text{éq 2.1-2}$$

$$\dot{\varepsilon}_p - \dot{p} \frac{\partial F}{\partial \sigma} = 0 \quad \text{éq 2.1-3}$$

$$\dot{\gamma}_p - \dot{p} \frac{\partial F}{\partial \tau} = 0 \quad \text{éq 2.1-4}$$

$$\left[ -\frac{3}{2} \frac{\partial F}{\partial \sigma} \left( Kx + Cs \frac{\partial F}{\partial \sigma} \right) - 2 \frac{\partial F}{\partial \tau} \left( Ky + Cs \frac{\partial F}{\partial \tau} \right) - HR - a D \alpha Z^{(\alpha-2)} \right. \\ \left. \left( \left( \varepsilon_p - \varepsilon_p^n \right) \frac{\partial F}{\partial \sigma} + \frac{4}{3} \left( \gamma_p - \gamma_p^n \right) \frac{\partial F}{\partial \tau} \right) \right] \dot{p} + \left[ \frac{3}{2} \frac{\partial F}{\partial \sigma} \left( Qx + C\varepsilon_p^n \right) + 2 \frac{\partial F}{\partial \tau} \left( Qy + C\gamma_p^n \right) + JR \right] \dot{\sigma}_p \\ = - \frac{\partial F}{\partial \sigma} \dot{\beta} \sigma_o - 2 \frac{\partial F}{\partial \tau} \dot{\beta} \tau_o \quad \text{éq 2.1-5}$$

$$\left[ 1 + JR + \frac{3C}{2U} \left( \frac{3}{2} C \left( \varepsilon_p s - \sigma_p \varepsilon_p^n \right) \varepsilon_p^n + 2C \left( s \gamma_p - \sigma_p \gamma_p^n \right) \gamma_p^n \right) \right] \dot{\sigma}_p \\ - \left[ HR + a D \alpha Z^{(\alpha-2)} \left( \left( \varepsilon_p - \varepsilon_p^n \right) \frac{\partial F}{\partial \sigma} + \frac{4}{3} \left( \gamma_p - \gamma_p^n \right) \frac{\partial F}{\partial \tau} \right) + KX \right. \\ \left. + 3 \frac{CS}{2U} \left( \frac{3}{2} C \left( s \varepsilon_p - \sigma_p \varepsilon_p^n \right) \frac{\partial F}{\partial \sigma} + 2C \left( s \gamma_p - \sigma_p \gamma_p^n \right) \frac{\partial F}{\partial \tau} \right) \right] \dot{p} = 0 \quad \text{éq 2.1-6}$$

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et

$$D = 1 - me^{-up} \quad \begin{cases} u = b \left( 1 - \frac{\sigma_p}{S} \right) \\ v = \frac{C_\infty - C}{C} \\ w = \frac{1 - D}{D} \\ C = C_\infty - C_1 e^{-up} \\ K = vu \quad Q = v \frac{bp}{s} \\ H = wu \quad J = w \frac{bp}{s} \end{cases} \quad \begin{cases} X = C \left( s \varepsilon_p - \sigma_p \varepsilon_p^n \right) \\ Y = C \left( s \gamma_p - \sigma_p \gamma_p^n \right) \\ U = \left[ \frac{9}{4} X^2 + 3 Y^2 \right]^{1/2} \\ R = D \left( a Z^\alpha + r0 \right) \\ Z = \left[ \left( \varepsilon_p - \varepsilon_p^n \right)^2 + \frac{4}{3} \left( \gamma_p - \gamma_p^n \right)^2 \right]^{1/2} \end{cases}$$

with the initial conditions:

$$\begin{cases} \beta(0) = \frac{R(0)}{(\sigma_o^2 + 3\tau_o^2)^{1/2}} \\ \varepsilon(0) = \beta(0) \frac{\sigma_o}{E} \\ \gamma(0) = \beta(0) \frac{\tau_o}{2\mu} \\ p(0) = \varepsilon_p(0) = \varepsilon_p^n = 0 \\ R(0) = (1-m) r_o = \sigma_p(o) \end{cases}$$

d'où  $\sigma(t=1) = \begin{bmatrix} 88. & 88. & 0 \\ 88. & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$

## 2.2 Results of reference

Values of  $\varepsilon, \gamma, \varepsilon_p, \gamma_p, p$  and  $\sigma_p$  to the nodes to  $t=1$  s.

## 2.3 Uncertainty on the solution

Uncertainty of library NAG.

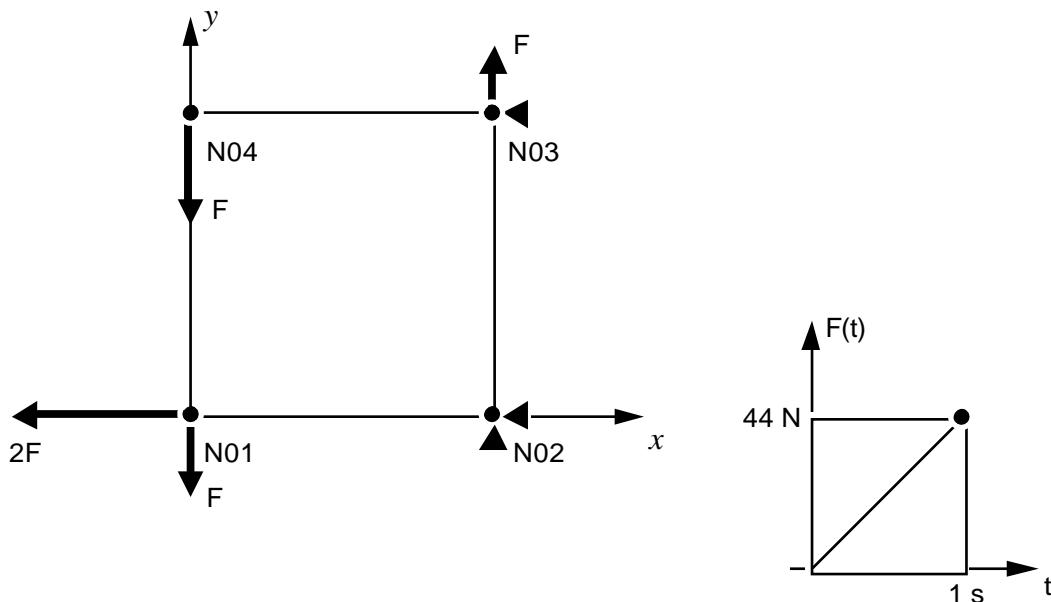
## 2.4 Bibliographical references

- 1) User's manual library NAG on CRAY.
- 2) S. ANDRIEUX - P. SCHOENBERGER - S. TAHERI: A three dimensional cyclic constitutive law for metals with has variable semi-DISCRET memory - HI - 71/8147 (1992)
- 3) P. GEYER - J.M. PROIX - P. SCHOENBERGER - S. TAHERI: Modelization of the phenomena of progressive strain - Collection of the internal notes of DER 93NB00153

## 3 Modelization A

### 3.1 Characteristic of modelization

Modelization in plane stresses 2D , c\_PLAN



### 3.2 Characteristic of the mesh

square Quadrangle to 4 nodes in plane stresses with:

$$\begin{aligned} \text{largeur} &= 1 \text{ mm} \\ \text{épaisseur} &= 1 \text{ mm} . \end{aligned}$$

### 3.3 Quantities tested and results

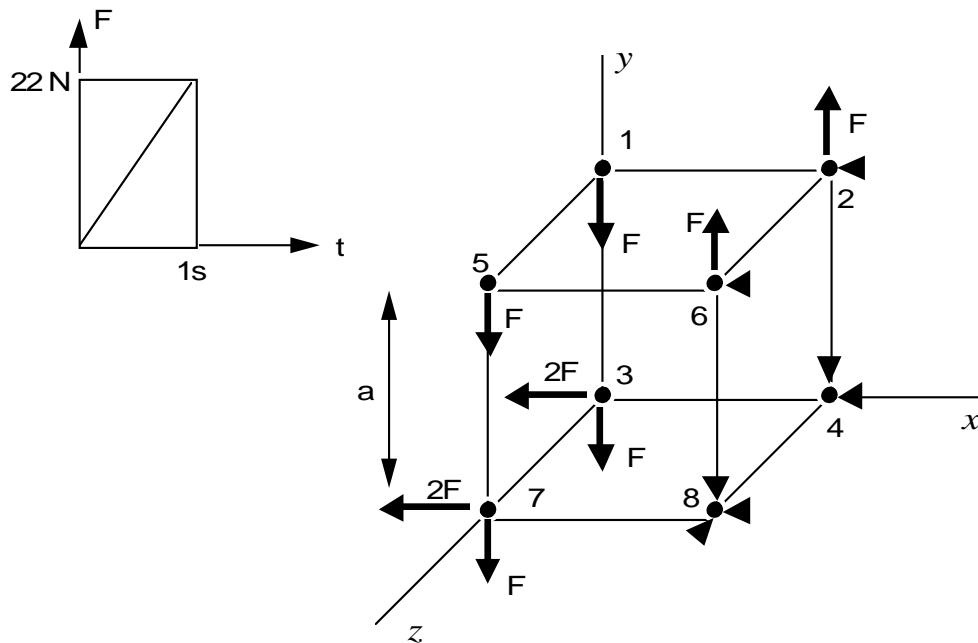
Identification	Reference	Test	Tolerance
$\varepsilon$ on NO4 to $t=1\text{s}$	0,01721	ANALYTIQUE	2,5%
$\gamma$ out of NO4 at $t=1\text{s}$	0,02573	ANALYTIQUE	2,5%
$\varepsilon_p$ on MA1 , Gauss point 4 with $t=1\text{s}$	0,01678	ANALYTIQUE	2,5%
$\gamma_p$ on MA1 , Gauss point 4 with $t=1\text{s}$	0,02515	ANALYTIQUE	2,5%
$\varepsilon_p$ out of NO4 to $t=1\text{s}$	0,01678	ANALYTIQUE	2,5%
$\gamma_p$ out of NO4 to $t=1\text{s}$	0,02515	ANALYTIQUE	2,5%
$\sigma_p$ out of NO1 to $t=1\text{s}$	176,0	ANALYTIQUE	0,10%

## 4 Modelization B

### 4.1 Characteristic of the modelization

Modelization 3D :

Cubic elementary with a grid using a hexahedron with 8 nodes.



### 4.2 Characteristics of mesh

1 nets HEXA8, width side  $a=1\text{ mm}$ .

### 4.3 Quantities tested and Values

#### 4.3.1 results tested

Identification	Reference	Test	Tolerance
$\varepsilon$ on NO4 to $t=1\text{s}$	0,01721	ANALYTIQUE	2,5%
$\gamma$ out of NO4 to $t=1\text{s}$	0,02573	ANALYTIQUE	2,5%
$\varepsilon_p$ on MA1 , Gauss point 1 with $t=1\text{s}$	0,01678	ANALYTIQUE	2,5%
$\gamma_p$ on MA1 , Gauss point 1 with $t=1\text{s}$	0,02515	ANALYTIQUE	2,5%
$\varepsilon_p$ out of NO4 to $t=1\text{s}$	0,01678	ANALYTIQUE	2,5%
$\gamma_p$ out of NO4 to $t=1\text{s}$	0,02515	ANALYTIQUE	2,5%
$\sigma_p$ out of NO1 to $t=1\text{s}$	176,0	ANALYTIQUE	0,10%
$p$ out of NO1 to $t=1\text{s}$	0,03	ANALYTIQUE	0,10%

One also tests the parameters of the data structure results:

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Identification	Reference	Test	Tolerance
INST for NUME_ORDRE= 6	1	ANALYTIQUE	0%
ITER_GLOB for NUME_ORDRE= 6	12	NON_REGRESSION	8

## 4.3.2 Remarks

the reduction in the tolerance on total convergence in displacement does not bring significant gain in accuracy.

The number of increments of load (6) led to a satisfactory accuracy of result.

## **5 Summary of the results**

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Good accuracy at the time of the comparison with NAG in spite of some difficulties of convergence with this mathematical library.