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## SSLV04 - Hollow roll in plane stresses

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### Summarized:

This test is drawn from Guide VPCS (test SSLV04/89) and has as an aim a hollow roll charged in internal pressure.

With this three-dimensional problem is dealt with various modelizations:

- in 3D : 9 modelizations (pentahedral, hexahedrons, tetrahedrons and pyramids, degrees 1 and 2),
- in 2D plane stresses: 4 modelizations (triangles and quadrangles degrees 1 and 2, quadrangles with 9 nodes),
- into 2D axisymmetric: 3 modelizations (triangles and quadrangles degrees 1 and 2, quadrangles with 9 nodes).

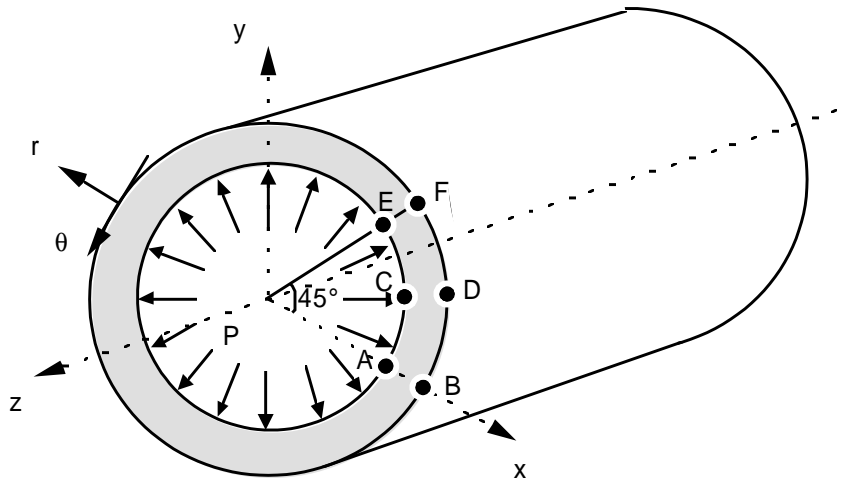
The features tested are:

- distributed pressure,
- basic effect (with fixed or variable pressure),
- imposed displacements,
- nodal stiffness matrixes
- , strains and nodal stresses
- , reactions (modelization K).

There are 16 modelizations.

## 1 Problem of reference

### 1.1 Geometry



Rayon interne  $a = 0.1$  m  
Rayon externe  $b = 0.2$  m

Coordinated of the points:

	<i>A</i>	<i>B</i>	<i>C</i>	<i>D</i>	<i>E</i>	<i>F</i>
<i>x</i>	0.100	0.200	$0.1 \cos(22.5)$	$0.2 \cos(22.5)$	$\sqrt{2}/2$	$\sqrt{2}$
<i>y</i>	0.	0.	$0.1 \sin(22.5)$	$0.2 \sin(22.5)$	$\sqrt{2}/2$	$\sqrt{2}$
<i>z</i>	0	0.	0.	0.	0.	0.

### 1.2 Material properties

the Young modulus of the material is equal to  $E = 2.10^5$  MPa .  
The Poisson's ratio is equal to  $\nu = 0.3$  .

### 1.3 Boundary conditions and loadings

internal Pressure:  
 $P = 60$  MPa

Pressure interns variable (modelization P only):  
 $P$  vary linearly  $60$  MPa with  $t = 1.s$   $120$  MPa with  $t = 2.s$

## 2 Reference solution

### 2.1 Method of calculating used for the reference solution

In plane stress (cylinder on free board at the ends)

$$\begin{aligned}\sigma_{zz} &= 0 \\ \sigma_{rr} &= P \frac{a^2}{b^2 - a^2} \left[ 1 - \frac{b^2}{r^2} \right] \\ \sigma_{\theta\theta} &= P \frac{a^2}{b^2 - a^2} \left[ 1 + \frac{b^2}{r^2} \right] \\ \sigma_{r\theta} &= 0 \\ u_r &= \frac{P}{E} \frac{a^2}{b^2 - a^2} \left[ (1 - \nu) + (1 + \nu) \frac{b^2}{r^2} \right] r \\ \varepsilon_{rr} &= \frac{P}{E} \frac{a^2}{b^2 - a^2} \left[ (1 - \nu) - (1 + \nu) \frac{b^2}{r^2} \right] \\ \varepsilon_{\theta\theta} &= \frac{u_r}{r}\end{aligned}$$

One obtains:

$$\begin{array}{ll} u_r = 59.10^{-6} & u_r = 40.10^{-6} \\ \sigma_{rr} = -60. & \sigma_{rr} = 0. \\ \sigma_{\theta\theta} = 100. & \sigma_{\theta\theta} = 40. \\ \text{for } r=0.1 : \sigma_{zz} = \sigma_{r\theta} = 0. & \text{; for } r=0.2 : \sigma_{zz} = \sigma_{r\theta} = 0. \\ \varepsilon_{rr} = -45.10^{-5} & \varepsilon_{rr} = -6.10^{-5} \\ \varepsilon_{\theta\theta} = 59.10^{-5} & \varepsilon_{\theta\theta} = 2.10^{-4} \end{array}$$

Transition in the system of Cartesian axes:

$$\begin{aligned}\sigma_{xx} &= \sigma_{rr} \cos^2 \theta + \sigma_{\theta\theta} \sin^2 \theta - 2 \sigma_{r\theta} \sin \theta \cos \theta \\ \sigma_{yy} &= \sigma_{rr} \sin^2 \theta + \sigma_{\theta\theta} \cos^2 \theta + 2 \sigma_{r\theta} \sin \theta \cos \theta \\ \sigma_{xy} &= \sigma_{rr} \sin \theta \cos \theta - \sigma_{\theta\theta} \sin \theta \cos \theta - 2 \sigma_{r\theta} (\cos^2 \theta - \sin^2 \theta)\end{aligned}$$

with:

- $\theta = 0^\circ$  at the points *A* and *B*,
- $\theta = 22.5^\circ$  at the points *C* and *D*,
- $\theta = 45^\circ$  at the points *E* and *F*.

### 2.2 Results of reference

Displacements  $(u, v)$  and stresses  $(\sigma_{xx}, \sigma_{yy}, \sigma_{zz}, \sigma_{xy})$  with the points *A, B, C, D, E, F*.

## 2.3 Bibliographical references

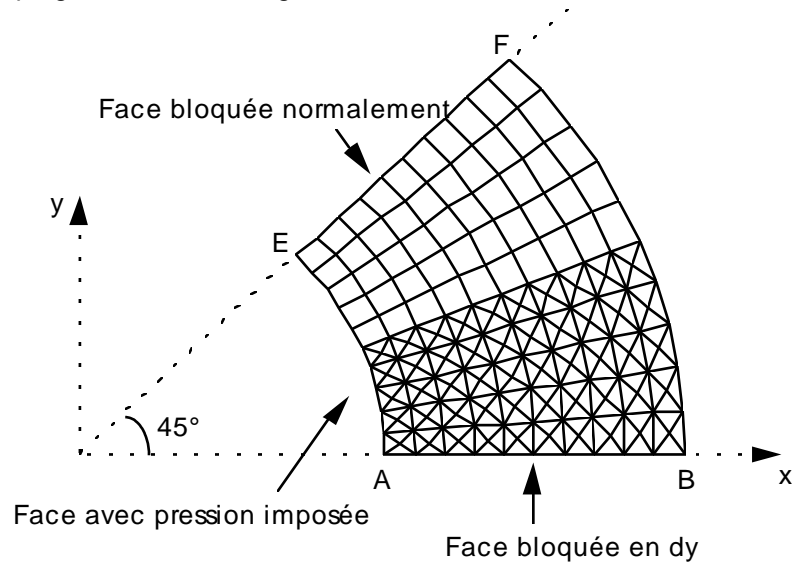
- 1 Guides VPCS. SSLV04/89
- 2 Y.C. FUNG. Foundations of solid mechanics. Prentice-hall, Inc. Englewood Cliffs. NJ. 1965  
p. 243 to 245.
- 3 J. COURBON. Strength of materials p 649

## 3 Modelization A

### 3.1 Characteristic of the modelization

Elements 3D (PENTA6 and HEXA8).

Mesh obtained by extrusion from a mesh 2D resembling the mesh below (30 elements in the radial direction with progressive coarsening and 15+15 elements in the circumferential direction).



Along the axis  $Z$  : 1 layer of elements  
total Thickness: 0.01m

Limiting conditions:

the node is outside the field of definition  
with a right profile of the EXCLU type  
node:  $F \quad u_z=0$

face  $AB$  blocked opposite  $dy$   
 $EF$  blocked normally

pressure on the face  $AE$   $p=60.$

Names the nodes:  $A=N993$   $B=N1443$   $C=N1$   
 $D=N31$   $E=N496$   $F=N495$

### 3.2 Characteristics of the mesh

Many nodes: 1922

Number of meshes and types: 900 PENTA6, 450 HEXA8 and 90 QUAD4 (sides internal skin).

## 3.3 Quantities tested and results

Localization	Quantity	Reference	Aster	% difference
<i>A</i>	<i>u</i>	5.9 10 <sup>-5</sup>	5.8950 10 <sup>-5</sup>	0.08
	<i>v</i>	0.	<i>eps</i>	-
	$\sigma_{xx}$	- 60.	- 59.2225	1.30
	$\sigma_{yy}$	100.	100.4159	0.42
	$\sigma_{zz}$	0.	0.3093	-
	$\sigma_{xy}$	0.	- 1.0442	-
	$\epsilon_{xx}$	- 4.5 10 <sup>-4</sup>	- 4.472 10 <sup>-4</sup>	0.62
	$\epsilon_{yy}$	5.9 10 <sup>-4</sup>	5.904 10 <sup>-4</sup>	0.08
	$\epsilon_{xy}$	0.	- 6.788 10 <sup>-5</sup>	-
<i>B</i>	<i>u</i>	4 10 <sup>-5</sup>	3.9959 10 <sup>-5</sup>	0.10
	<i>v</i>	0.	<i>eps</i>	-
	$\sigma_{xx}$	0.	- 1.7246	-
	$\sigma_{yy}$	40.	39.2451	1.89
	$\sigma_{zz}$	0.	- 0.3761	-
	$\sigma_{xy}$	0.	- 0.2659	-
	$\epsilon_{xx}$	- 0.6 10 <sup>-4</sup>	- 6.692 10 <sup>-5</sup>	11.54
	$\epsilon_{yy}$	2. 10 <sup>-4</sup>	1.994 10 <sup>-4</sup>	0.31
	$\epsilon_{xy}$	0.	- 1.728 10 <sup>-6</sup>	-
<i>E</i>	<i>u</i>	4.17193 10 <sup>-5</sup>	4.1708 10 <sup>-5</sup>	0.03
	<i>v</i>	4.17193 10 <sup>-5</sup>	4.1708 10 <sup>-5</sup>	0.03
	$\sigma_{xx}$	20.	19.0824	4.59
	$\sigma_{yy}$	20.	21.1394	5.70
	$\sigma_{zz}$	0.	0.0870	-
	$\sigma_{xy}$	- 80.	- 79.8831	0.15
	$\epsilon_{xx}$	0.7 10 <sup>-4</sup>	0.636 10 <sup>-4</sup>	9.18
	$\epsilon_{yy}$	0.7 10 <sup>-4</sup>	0.769 10 <sup>-4</sup>	9.92
	$\epsilon_{xy}$	- 5.2 10 <sup>-4</sup>	- 5.192 10 <sup>-4</sup>	0.15
<i>F</i>	<i>u</i>	2.82843 10 <sup>-5</sup>	2.8302 10 <sup>-5</sup>	0.06
	<i>v</i>	2.82843 10 <sup>-5</sup>	2.8302 10 <sup>-5</sup>	0.06
	$\sigma_{xx}$	20.	18.9528	5.24
	$\sigma_{yy}$	20.	19.9104	0.45
	$\sigma_{zz}$	0.	0.1198	-
	$\sigma_{xy}$	- 20.	- 20.1809	0.90
	$\epsilon_{xx}$	0.7 10 <sup>-4</sup>	0.647 10 <sup>-4</sup>	7.54
	$\epsilon_{yy}$	0.7 10 <sup>-4</sup>	0.709 10 <sup>-4</sup>	1.35
	$\epsilon_{xy}$	- 1.3 10 <sup>-4</sup>	- 1.312 10 <sup>-4</sup>	0.90

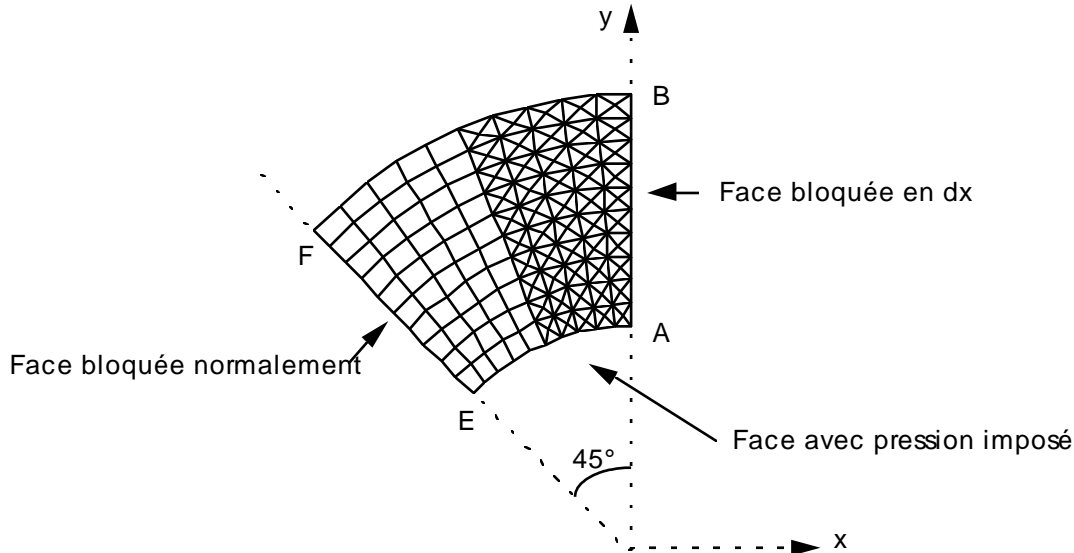
Localization	Quantity	Reference	Tolerance
<b>Nets M1380, not A</b>			
SIRO_ELEM	<i>SIG_NX</i>	60.0	2.0%
Normal stress with the face of the element	<i>SIG_NY</i>	0.0.1.0.0.0	
	<i>SIG_NZ</i>		0.01
	<i>SIG_N</i>	-60.0	2.0%
SIRO_ELEM	<i>SIG_TX</i>	0.0	0.01
Shear stress in the plane of the element	<i>SIG_TY</i>	0.0	1.0%
	<i>SIG_TZ</i>	0.0.1.0	
SIRO_ELEM	<i>SIG_T1X</i>	0.0	0.01
First value of the stress tangential in the plane of the element	<i>SIG_T1Y</i>	0.0	0.01
	<i>SIG_T1Z</i>	0.0.1.0.0.0	
	<i>SIG_T1</i>		1.0
SIRO_ELEM	<i>SIG_T2X</i>	0.0.2.0	
Second value of the tangential stress 1.0% in the plane of the element	<i>SIG_T2Y</i>		-100.0
	<i>SIG_T2Z</i>	0.0	0.01
	<i>SIG_T2</i>	100.0	1.0%
<b>Nets M1351, not E</b>			
SIRO_ELEM	<i>SIG_NX</i>	42.426	1.5%
Normal stress with the face of the element	<i>SIG_NY</i>	42.426	2.0%
	<i>SIG_NZ</i>	0.0	0.01
	<i>SIG_N</i>	-60.0	1.0%
SIRO_ELEM	<i>SIG_TX</i>	0.0	1.0
Shear stress in the plane of the element	<i>SIG_TY</i>	0.0	1.0.0.0.0.2
	<i>SIG_TZ</i>		
SIRO_ELEM	<i>SIG_T1X</i>	0.0	0.01
First value of the stress tangential in the plane of the element	<i>SIG_T1Y</i>	0.0	0.01
	<i>SIG_T1Z</i>	0.0.0.1.0.0	
	<i>SIG_T1</i>		0.2
SIRO_ELEM	<i>SIG_T2X</i>	70.711	1.5%
Second value of the tangential stress 1.5% in the plane of the element	<i>SIG_T2Y</i>		-70.711
	<i>SIG_T2Z</i>	0.0	0.01
	<i>SIG_T2</i>	100.0	1.0%

## 4 Modelization B

### 4.1 Characteristic of the modelization

Elements 3D (PENTA15 and HEXA20).

Mesh obtained by extrusion starting from the mesh 2D below (modelization F)



Along the axis  $Z$  : 2 layers of elements  
total Thickness: 0.01m

Limiting conditions:

node  $F = u_z = 0$

face  $AB$  blocked opposite  $dx$

$EF$  blocked normally

pressure on the face  $AE$   $p = 60$ .

Names the nodes:

$A = NO2$        $B = NO361$        $C = NO121$   
 $D = NO584$      $E = NO155$        $F = NO503$

### 4.2 Characteristics of the mesh

Many nodes: 2115

Number of meshes and types: 400 PENTA15, 100 HEXA20 40 QUAD8 (sides skin interns)



## 4.3 Quantities tested and results

Localization	Quantity	Reference	Aster	% difference
<i>A</i>	<i>u</i>	0.	eps	-
	<i>v</i>	5.9 10-5	5.8944 10-5	-0.09
	$\sigma_{xx}$	100.	99.6056	-0.39
	$\sigma_{vv}$	-60.	-59.4473	-0.92
	$\sigma_{zz}$	0.	0.0196	-
	$\sigma_{xv}$	0.	0.2481	-
	$\varepsilon_{xx}$	5.9 10-4	5.87 10-4	-0.48
	$\varepsilon_{vv}$	-4.5 10-4	-4.47 10-4	-0.74
	$\varepsilon_{xv}$	0.	1.61 10 <sup>-6</sup>	-
	<i>B</i>	<i>u</i>	0.	eps
<i>v</i>		4 10-5	3.9974 10-5	-0.07
$\sigma_{xx}$		40.	39.9711	0.07
$\sigma_{vv}$		0.	0.0781	-
$\sigma_{zz}$		0.	5.7992 10-3	-
$\sigma_{xv}$		0.	-0.0182	-
$\varepsilon_{xx}$		2. 10-4	1.997 10-4	-0.13
$\varepsilon_{vv}$		-0.6. 10-4	-0.596 10-4	-0.67
$\varepsilon_{xv}$		0.	-1.1810-7	-
<i>E</i>		<i>u</i>	4.17193 10-5	4.1680 10-5
	<i>v</i>	4.17193 10-5	4.1680 10-5	-0.09
	$\sigma_{xx}$	20.	20.0515	0.26
	$\sigma_{vv}$	20.	20.0264	0.13
	$\sigma_{zz}$	0.	-0.0155	-
	$\sigma_{xv}$	80.	79.7918	-0.26
	$\varepsilon_{xx}$	0.7 10-4	0.702 10-4	0.34
	$\varepsilon_{vv}$	0.7 10-4	0.701 10-4	0.11
	$\varepsilon_{xv}$	5.2 10 <sup>-4</sup>	5.19 10 <sup>-4</sup>	-0.26
	<i>F</i>	<i>u</i>	-2.82843 10 <sup>-5</sup>	-2.82656 10 <sup>-5</sup>
<i>v</i>		2.82843 10-5	2.82656 10-5	-0.07
$\sigma_{xx}$		20.	20.0099	0.05
$\sigma_{vv}$		20.	19.9980	-0.01
$\sigma_{zz}$		0.	-3.90 10-4	-
$\sigma_{xv}$		20.	20.0122	0.06
$\varepsilon_{xx}$		0.7 10-4	0.7005 10-4	0.08
$\varepsilon_{vv}$		0.7 10-4	0.6997 10-4	-0.03
$\varepsilon_{xv}$		-1.3 10-4	-1.3008 10-4	0.06

Localization	Quantity	Reference	Tolerance
<b>Nets MA751, not A</b>			
SIRO_ELEM	<i>SIG_NX</i>	0.0	3.
Normal stress with the face of the element	<i>SIG_NY</i>	60.0	0.5%
	<i>SIG_NZ</i>	0.0	0.01
	SIRO_ELEM	<i>SIG_TX</i>	0.0.0.1
Shear stress in the plane of the element	<i>SIG_TY</i>	0.0.0.1	
	<i>SIG_TZ</i>	0.0.0.1	
	SIRO_ELEM	<i>SIG_T1X</i>	0.0
First value of the stress tangential in the plane of the element	<i>SIG_T1Y</i>	0.0	0.01
	<i>SIG_T1Z</i>	0.0	0.05
	SIRO_ELEM	<i>SIG_T2X</i>	100.0
Second value of tangential stress 0.0.4.5 in the plane of the element	<i>SIG_T2Y</i>		
	<i>SIG_T2Z</i>	0.0	0.20
<b>Mesh MA769, not E</b>			
SIRO_ELEM	<i>SIG_NX</i>	-42.426	6.0%
Normal stress with the face of the element	<i>SIG_NY</i>	42.426	4.0%
	<i>SIG_NZ</i>	0.0	0.01
	SIRO_ELEM	<i>SIG_TX</i>	0.0
Shear stress in the plane of the element	<i>SIG_TY</i>	0.0	0.01
	<i>SIG_TZ</i>	0.0	0.03
	SIRO_ELEM	<i>SIG_T1X</i>	0.0
First value of the stress tangential in the plane of the element	<i>SIG_T1Y</i>	0.0	0.01
	<i>SIG_T1Z</i>	0.0	0.01
	SIRO_ELEM	<i>SIG_T2X</i>	70.711
Second value of tangential stress 4.5% in the plane of the element	<i>SIG_T2Y</i>		70.711
	<i>SIG_T2Z</i>	0.0.0.1	

## 5 Modelization C

### 5.1 Characteristics of the modelization

Elements 3D (TETRA4).  
 $AB$  is on the axis  $OX$

Cutting: 21 equidistant nodes on the equidistant  $AB$  segments  
 $CD$ ,  $EF$   
and 21 nodes on the arcs  $ACE$  and  $BDF$

Along the axis  $Z$  : 1 layer of elements  
total Thickness: 0.01m

Limiting conditions:

the node is outside the field of  
definition with a right profile of  
the EXCLU type node:  $F$   
 $u_z=0$

face  $AB$  blocked opposite  $dy$   
 $EF$  blocked normally

pressure on the face  $AE$   $p=60$ .

Names the nodes:  $A=N165$   $B=N4$   $C=N209$   
 $D=N82$   $E=N244$   $F=N1068$

### 5.2 Characteristics of the mesh

Many nodes: 1115  
Number of meshes and types: 3724 TETRA4 and 1760 TRIA3 (sides skin interns)

## 5.3 Quantities tested and results

Localization	Quantity	Reference	Aster	% difference
<i>A</i>	<i>u</i>	5.9 10 <sup>-5</sup>	5.8901 10 <sup>-5</sup>	- 0.17
	<i>v</i>	0.	eps	-
	$\sigma_{xx}$	- 60.	- 57.2290	- 4.62
	$\sigma_{vv}$	100.	97.8711	- 2.13
	$\sigma_{zz}$	0.	0.0568	-
	$\sigma_{xv}$	0.	- 2.6589	-
	$\varepsilon_{xx}$	- 4.5 10 <sup>-4</sup>	- 4.33 10 <sup>-4</sup>	- 3.77
	$\varepsilon_{vv}$	5.9 10 <sup>-4</sup>	5.75 10 <sup>-4</sup>	- 2.52
	$\varepsilon_{xv}$	0.	- 1.73 10 <sup>-5</sup>	-
<i>B</i>	<i>u</i>	4 10 <sup>-5</sup>	3.9878 10 <sup>-5</sup>	- 0.30
	<i>v</i>	0.	eps	-
	$\sigma_{xx}$	0.	- 1.5296	-
	$\sigma_{vv}$	40.	40.9839	2.46
	$\sigma_{zz}$	0.	- 0.1006	-
	$\sigma_{xv}$	0.	- 0.8513	-
	$\varepsilon_{xx}$	- 0.6 10 <sup>-4</sup>	- 6.897 10 <sup>-4</sup>	14.95
	$\varepsilon_{vv}$	2. 10 <sup>-4</sup>	2.074 10 <sup>-4</sup>	3.68
	$\varepsilon_{xv}$	0.	- 5.534 10 <sup>-5</sup>	-
<i>E</i>	<i>u</i>	4.17193 10 <sup>-5</sup>	4.1655 10 <sup>-5</sup>	- 0.15
	<i>v</i>	4.17193 10 <sup>-5</sup>	4.1655 10 <sup>-5</sup>	- 0.15
	$\sigma_{xx}$	20.	17.9096	- 10.45
	$\sigma_{vv}$	20.	21.8929	9.46
	$\sigma_{zz}$	0.	- 0.3679	-
	$\sigma_{xv}$	- 80.	- 77.6897	- 2.89
	$\varepsilon_{xx}$	0.7 10 <sup>-4</sup>	0.573 10 <sup>-4</sup>	- 18.20
	$\varepsilon_{vv}$	0.7 10 <sup>-4</sup>	0.832 10 <sup>-4</sup>	18.79
	$\varepsilon_{xv}$	- 5.2 10 <sup>-4</sup>	- 5.050 10 <sup>-4</sup>	- 2.89
<i>F</i>	<i>u</i>	2.82843 10 <sup>-5</sup>	2.8251 10 <sup>-5</sup>	- 0.12
	<i>v</i>	2.82843 10 <sup>-5</sup>	2.8251 10 <sup>-5</sup>	- 0.12
	$\sigma_{xx}$	20.	18.4444	- 7.78
	$\sigma_{vv}$	20.	19.8876	- 0.56
	$\sigma_{zz}$	0.	- 0.3910	-
	$\sigma_{xv}$	- 20.	- 20.1631	0.81
	$\varepsilon_{xx}$	0.7 10 <sup>-4</sup>	0.630 10 <sup>-4</sup>	- 10.05
	$\varepsilon_{vv}$	0.7 10 <sup>-4</sup>	0.723 10 <sup>-4</sup>	3.35
	$\varepsilon_{xv}$	- 1.3 10 <sup>-4</sup>	- 1.311 10 <sup>-4</sup>	0.81

Localization	Quantity	Reference	Tolerance
<b>Nets M5444, not A</b>			
SIRO_ELEM	<i>SIG_NX</i>	60.0	8.0%
Normal stress with the face of the element	<i>SIG_NY</i>	0.0.1.5.0.0	
	<i>SIG_NZ</i>		0.1
	SIRO_ELEM	<i>SIG_TX</i>	0.0.0.1
Shear stress in the plane of the element	<i>SIG_TY</i>	0.0	1.0
	<i>SIG_TZ</i>	0.0.1.0	
	SIRO_ELEM	<i>SIG_T1X</i>	0.0
First value of the stress tangential in the plane of the element	<i>SIG_T1Y</i>	0.0	0.01
	<i>SIG_T1Z</i>	0.0.1.5	
	SIRO_ELEM	<i>SIG_T2X</i>	0.0.2.5
Second value of tangential stress 2.0% in the plane of the element	<i>SIG_T2Y</i>		-100.0
	<i>SIG_T2Z</i>	0.0	0.20
	<b>M5404 Mesh, not E</b>		
SIRO_ELEM	<i>SIG_NX</i>	42.426	6.0%
Normal stress with the face of the element	<i>SIG_NY</i>	42.426	9.0%
	<i>SIG_NZ</i>	0.0	1.00
	SIRO_ELEM	<i>SIG_TX</i>	0.0
Shear stress in the plane of the element	<i>SIG_TY</i>	0.0	1.0
	<i>SIG_TZ</i>	0.0.1.0	
	SIRO_ELEM	<i>SIG_T1X</i>	0.0
First value of stress tangential in the plane of the element	<i>SIG_T1Y</i>	0.0	0.01
	<i>SIG_T1Z</i>	0.0	1.50
	SIRO_ELEM	<i>SIG_T2X</i>	-70.711
Second value of tangential stress 4.0% in the plane of the element	<i>SIG_T2Y</i>		70.711
	<i>SIG_T2Z</i>	0.0	0.10

## 6 Modelization D

### 6.1 Characteristic of the modelization

Element 3D (TETRA10).

$AB$  is on the axis  $OX$

Cutting: 11 equidistant nodes on the equidistant  $AB$  segments  
 $CD$ ,  $EF$   
and 11 nodes on the arcs  $ACE$  and  $BDF$

Along the axis  $Z$  : 1 layer of elements  
total Thickness: 0.01m

Limiting conditions:

the node is outside the field of  
definition with a right profile of  
the EXCLU type node:  $F$

$$u_z = 0$$

face  $AB$  blocked opposite  $dy$

$EF$  blocked normally

pressure on the face  $AE$   $p = 60$ .

Names the nodes:  $A = N184$        $B = N4$        $C = N207$   
 $D = N50$        $E = N22$        $F = N726$

### 6.2 Characteristics of the mesh

Many nodes: 1395

Number of meshes and types: 652 TETRA10 and 480 TRIA6 (sides skin interns)

## 6.3 Quantities tested and results

Localization	Quantity	Reference	Aster	% difference
<i>A</i>	<i>u</i>	5.9 10 <sup>-5</sup>	5.8974 10 <sup>-5</sup>	- 0.04
	<i>v</i>	0.	<i>eps</i>	-
	$\sigma_{xx}$	- 60.	- 60.3816	0.64
	$\sigma_{vv}$	100.	99.1907	- 0.81
	$\sigma_{zz}$	0.	- 0.9707	-
	$\sigma_{xv}$	0.	- 0.2979	-
	$\varepsilon_{xx}$	- 4.5 10 <sup>-4</sup>	- 4.49 10 <sup>-4</sup>	- 0.17
	$\varepsilon_{vv}$	5.9 10 <sup>-4</sup>	5.88 10 <sup>-4</sup>	- 0.34
	$\varepsilon_{xv}$	0.	- 1.94 10 <sup>-6</sup>	-
<i>B</i>	<i>u</i>	4 10 <sup>-5</sup>	3.9989 10 <sup>-5</sup>	- 0.03
	<i>v</i>	0.	<i>eps</i>	-
	$\sigma_{xx}$	0.	0.0388	-
	$\sigma_{vv}$	40.	40.0725	0.18
	$\sigma_{zz}$	0.	- 0.0046	-
	$\sigma_{xv}$	0.	0.1634	-
	$\varepsilon_{xx}$	- 0.6 10 <sup>-4</sup>	- 0.599 10 <sup>-4</sup>	- 0.15
	$\varepsilon_{vv}$	2. 10 <sup>-4</sup>	2.003 10 <sup>-4</sup>	0.16
	$\varepsilon_{xv}$	0.	1.062 10 <sup>-6</sup>	-
<i>E</i>	<i>u</i>	4.17193 10 <sup>-5</sup>	4.17021 10 <sup>-5</sup>	0.04
	<i>v</i>	4.17193 10 <sup>-5</sup>	4.17021 10 <sup>-5</sup>	0.04
	$\sigma_{xx}$	20.	19.1178	- 4.41
	$\sigma_{vv}$	20.	19.6399	- 1.80
	$\sigma_{zz}$	0.	- 1.0206	-
	$\sigma_{xv}$	- 80.	- 79.7804	- 0.27
	$\varepsilon_{xx}$	0.7 10 <sup>-4</sup>	0.677 10 <sup>-4</sup>	- 3.34
	$\varepsilon_{vv}$	0.7 10 <sup>-4</sup>	0.711 10 <sup>-4</sup>	1.50
	$\varepsilon_{xv}$	- 5.2 10 <sup>-4</sup>	- 5.186 10 <sup>-4</sup>	- 0.27
<i>F</i>	<i>u</i>	2.82843 10 <sup>-5</sup>	2.82718 10 <sup>-5</sup>	- 0.04
	<i>v</i>	2.82843 10 <sup>-5</sup>	2.82718 10 <sup>-5</sup>	- 0.04
	$\sigma_{xx}$	20.	20.1903	0.95
	$\sigma_{vv}$	20.	19.9023	- 0.49
	$\sigma_{zz}$	0.	- 0.0016	-
	$\sigma_{xv}$	- 20.	- 20.0570	0.28
	$\varepsilon_{xx}$	0.7 10 <sup>-4</sup>	0.711 10 <sup>-4</sup>	1.57
	$\varepsilon_{vv}$	0.7 10 <sup>-4</sup>	0.692 10 <sup>-4</sup>	- 1.10
	$\varepsilon_{xv}$	- 1.3 10 <sup>-4</sup>	- 1.304 10 <sup>-4</sup>	0.28

Localization	Quantity	Reference	Tolerance
<b>Nets M1111, not A</b>			
SIRO_ELEM	<i>SIG_NX</i>	60.0	1.0%
Normal stress with the face of the element	<i>SIG_NY</i>	0.0.3.0.0.0	
	<i>SIG_NZ</i>		1.0
	SIRO_ELEM	<i>SIG_TX</i>	0.0
Shear stress in the plane of the element	<i>SIG_TY</i>	0.0.2.5	
	<i>SIG_TZ</i>	0.0.1.0	
	SIRO_ELEM	<i>SIG_T1X</i>	0.0
First value principal of the stress tangential in the plane of the element	<i>SIG_T1Y</i>	0.0	0.01
	<i>SIG_T1Z</i>	0.0.1.0	
	SIRO_ELEM	<i>SIG_T2X</i>	0.0.4.5
Second value principal of the tangential stress 1.0% in the plane of element	<i>SIG_T2Y</i>		-100.0
	<i>SIG_T2Z</i>	0.0.0.1	
	<b>Nets M1093, not E</b>		
SIRO_ELEM	<i>SIG_NX</i>	42.426	14%
Normal stress with the face of the element	<i>SIG_NY</i>	42.426	5.0%
	<i>SIG_NZ</i>	0.0.1.0	
	SIRO_ELEM	<i>SIG_TX</i>	0.0
Shear stress in the plane of the element	<i>SIG_TY</i>	0.0	2.0
	<i>SIG_TZ</i>	0.0.1.0	
	SIRO_ELEM	<i>SIG_T1X</i>	0.0
First value principal stress tangential in the plane of the element	<i>SIG_T1Y</i>	0.0	0.01
	<i>SIG_T1Z</i>	0.0.1.5	
	SIRO_ELEM	<i>SIG_T2X</i>	-70.711
Second principal value of tangential stress 4.0% in the plane of the element	<i>SIG_T2Y</i>		70.711
	<i>SIG_T2Z</i>	0.0.2.0	

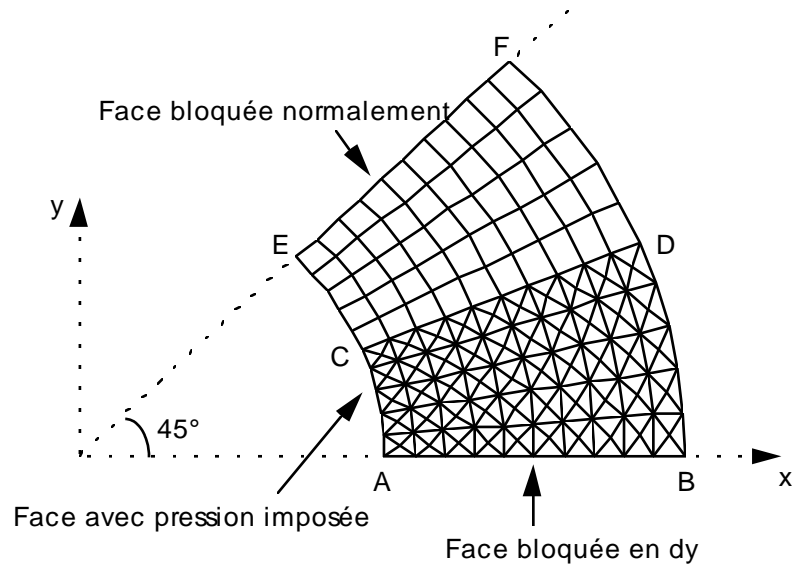


## 7 Modelization E

### 7.1 Characteristic of the modelization

Elements C\_PLAN (TRIA3 + QUAD4)

Mesh 2D resembling the mesh below (30 elements in the radial direction with progressive coarsening and 15+15 elements in the circumferential direction).



Limiting conditions:

side  $AB$  blocked in  $dy$   
side  $EF$  normally blocked  
pressure on  $AE$   $p=60$ .

Names of the nodes:       $A = N1$                        $B = N451$                        $C = N496$   
                                          $D = N495$                        $E = N990$                        $F = N989$

### 7.2 Characteristics of the mesh

Many nodes: 961  
Number of meshes and types: 900 TRIA3, 450 QUAD4

### 7.3

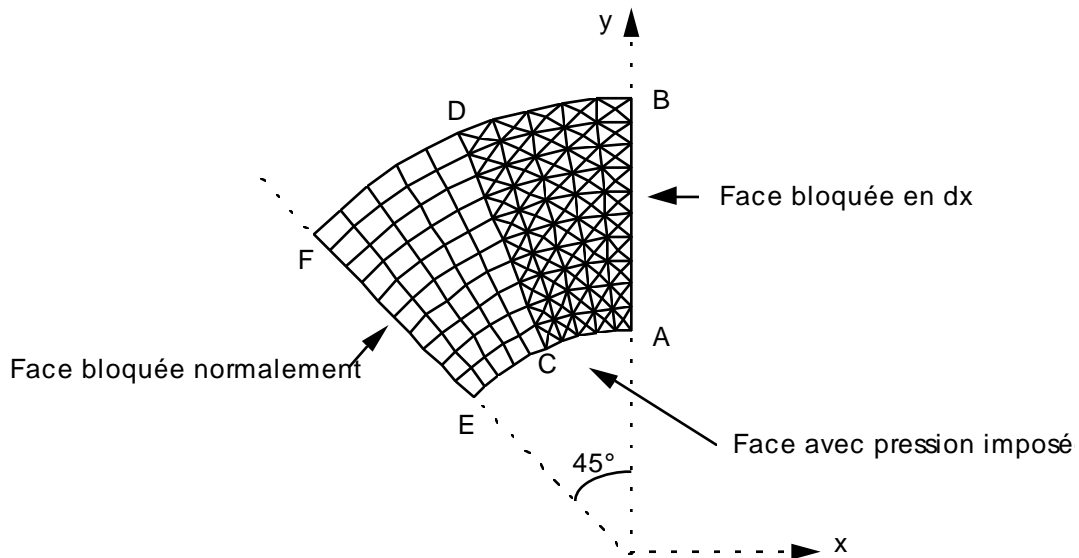
## 7.4 Quantities tested and results

Localization	Quantity	Reference	Aster	% difference
<i>A</i>	<i>u</i>	5.9 10 <sup>-5</sup>	5.8957 10 <sup>-5</sup>	- 0.07
	<i>v</i>	0.	eps	-
	$\sigma_{xx}$	- 60.	- 59.3645	- 1.06
	$\sigma_{vv}$	100.	100.2653	0.26
	$\sigma_{zz}$	0.	0.	-
	$\sigma_{xv}$	0.	- 1.0472	-
	$\varepsilon_{xx}$	- 4.5 10 <sup>-4</sup>	- 4.472 10 <sup>-4</sup>	- 0.62
	$\varepsilon_{vv}$	5.9 10 <sup>-4</sup>	5.904 10 <sup>-4</sup>	0.06
	$\varepsilon_{xv}$	0.	- 6.807 10 <sup>-6</sup>	-
<i>B</i>	<i>u</i>	4. 10 <sup>-5</sup>	3.9965 10 <sup>-5</sup>	- 0.09
	<i>v</i>	0.	eps	-
	$\sigma_{xx}$	0.	- 1.4986	-
	$\sigma_{vv}$	40.	39.4415	- 1.40
	$\sigma_{zz}$	0.	0.	-
	$\sigma_{xv}$	0.	- 0.2658	-
	$\varepsilon_{xx}$	- 0.6 10 <sup>-4</sup>	- 0.667 10 <sup>-5</sup>	11.09
	$\varepsilon_{vv}$	2. 10 <sup>-4</sup>	1.995 10 <sup>-4</sup>	- 0.27
	$\varepsilon_{xv}$	0.	- 1.728 10 <sup>-6</sup>	-
<i>E</i>	<i>u</i>	4.17193 10 <sup>-5</sup>	4.17101 10 <sup>-5</sup>	- 0.02
	<i>v</i>	4.17193 10 <sup>-5</sup>	4.17101 10 <sup>-5</sup>	- 0.02
	$\sigma_{xx}$	20.	19.0706	- 4.65
	$\sigma_{vv}$	20.	21.1354	5.68
	$\sigma_{zz}$	0.	0.	-
	$\sigma_{xv}$	- 80.	- 79.8720	- 0.16
	$\varepsilon_{xx}$	0.7 10 <sup>-4</sup>	0.636 10 <sup>-4</sup>	- 9.07
	$\varepsilon_{vv}$	0.7 10 <sup>-4</sup>	0.771 10 <sup>-4</sup>	10.10
	$\varepsilon_{xv}$	- 5.2 10 <sup>-4</sup>	- 5.192 10 <sup>-4</sup>	- 0.16
<i>F</i>	<i>u</i>	2.82843 10 <sup>-5</sup>	2.82996 10 <sup>-5</sup>	0.05
	<i>v</i>	2.82843 10 <sup>-5</sup>	2.82996 10 <sup>-5</sup>	0.05
	$\sigma_{xx}$	20.	18.9626	- 5.19
	$\sigma_{vv}$	20.	19.8483	- 0.76
	$\sigma_{zz}$	0.	0.	-
	$\sigma_{xv}$	- 20.	- 20.2466	1.23
	$\varepsilon_{xx}$	0.7 10 <sup>-4</sup>	0.650 10 <sup>-4</sup>	- 7.08
	$\varepsilon_{vv}$	0.7 10 <sup>-4</sup>	0.708 10 <sup>-4</sup>	1.14
	$\varepsilon_{xv}$	- 1.3 10 <sup>-4</sup>	- 1.316 10 <sup>-4</sup>	1.23

## 8 Modelization F

### 8.1 Characteristic of the modelization

C\_plan Elements (QUAD8 + TRIA6)



limiting Conditions:

side  $AB$  blocked in  $dx$   
side  $EF$  normally blocked  
pressure on  $AE$   $p=60$ .

Names of the nodes:       $A=N2$                $B=N361$                $C=N121$   
                                  $D=N584$                $E=N155$                $F=N503$

### 8.2 Characteristics of the mesh

Many nodes: 591  
Number of meshes and types: 200 TRIA6, 50 QUAD8

### 8.3

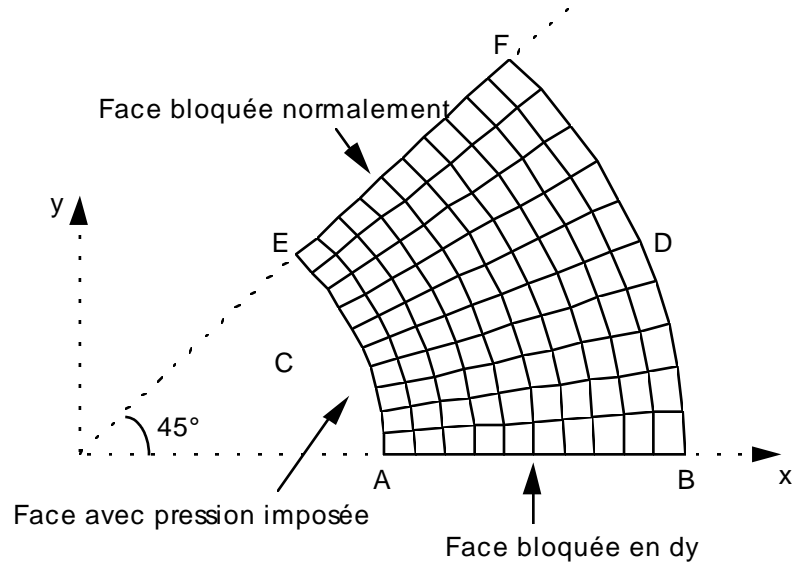
## 8.4 Quantities tested and results

Localization	Quantity	Reference	Aster	% difference
<i>A</i>	<i>u</i>	0.	0.	-
	<i>v</i>	5.9 10 <sup>-5</sup>	5.8945 10 <sup>-5</sup>	- 0.09
	$\sigma_{xx}$	100.	99.6095	- 0.39
	$\sigma_{yy}$	- 60.	- 59.4620	- 0.90
	$\sigma_{zz}$	0.	0.	-
	$\sigma_{xy}$	0.	0.2441	-
	$\varepsilon_{xx}$	5.9 10 <sup>-4</sup>	5.872 10 <sup>-4</sup>	- 0.47
	$\varepsilon_{yy}$	- 4.5 10 <sup>-4</sup>	- 4.467 10 <sup>-4</sup>	- 0.73
	$\varepsilon_{xy}$	0.	1.586 10 <sup>-6</sup>	-
<i>B</i>	<i>u</i>	0.	eps	-
	<i>v</i>	4 10 <sup>-5</sup>	3.9974 10 <sup>-5</sup>	- 0.07
	$\sigma_{xx}$	40.	39.9774	- 0.06
	$\sigma_{yy}$	0.	0.0786	-
	$\sigma_{zz}$	0.	0.	-
	$\sigma_{xy}$	0.	- 0.0181	-
	$\varepsilon_{xx}$	2. 10 <sup>-4</sup>	1.998 10 <sup>-4</sup>	- 0.11
	$\varepsilon_{yy}$	- 0.6 10 <sup>-4</sup>	- 0.596 10 <sup>-4</sup>	- 0.67
	$\varepsilon_{xy}$	0.	- 1.176 10 <sup>-7</sup>	-
<i>E</i>	<i>u</i>	-4.17193 10 <sup>-5</sup>	-4.16814 10 <sup>-5</sup>	- 0.09
	<i>v</i>	4.17193 10 <sup>-5</sup>	4.16814 10 <sup>-5</sup>	- 0.09
	$\sigma_{xx}$	20.	20.0024	0.01
	$\sigma_{yy}$	20.	20.0045	0.02
	$\sigma_{zz}$	0.	0.	-
	$\sigma_{xy}$	80.	79.8164	- 0.23
	$\varepsilon_{xx}$	0.7 10 <sup>-4</sup>	0.7001 10 <sup>-4</sup>	0.01
	$\varepsilon_{yy}$	0.7 10 <sup>-4</sup>	0.7002 10 <sup>-4</sup>	0.03
	$\varepsilon_{xy}$	5.2 10 <sup>-4</sup>	5.188 10 <sup>-4</sup>	- 0.23
<i>F</i>	<i>u</i>	- 2.82843 10 <sup>-5</sup>	- 2.82655 10 <sup>-5</sup>	- 0.07
	<i>v</i>	2.82843 10 <sup>-5</sup>	2.82655 10 <sup>-5</sup>	- 0.07
	$\sigma_{xx}$	20.	20.0083	0.04
	$\sigma_{yy}$	20.	19.9915	- 0.04
	$\sigma_{zz}$	0.	0.	-
	$\sigma_{xy}$	20.	20.0138	0.07
	$\varepsilon_{xx}$	0.7 10 <sup>-4</sup>	0.7005 10 <sup>-4</sup>	0.08
	$\varepsilon_{yy}$	0.7 10 <sup>-4</sup>	0.6995 10 <sup>-4</sup>	- 0.08
	$\varepsilon_{xy}$	- 1.3 10 <sup>-4</sup>	1.3009 10 <sup>-4</sup>	0.07

## 9 Modelization G

### 9.1 Characteristic of the modelization

Modelization C\_PLAN (QUAD9)



limiting Conditions:

side  $AB$  blocked in  $dy$   
side  $EF$  normally blocked  
pressure on  $AE$   $p=60$ .

Names of the nodes:       $A=N1$                        $B=N347$                        $C=N21$   
                                          $D=N432$                        $E=N39$                        $F=N229$

### 9.2 Characteristics of the mesh

Many nodes: 441  
Number of meshes and types: 100 QUAD9

### 9.3

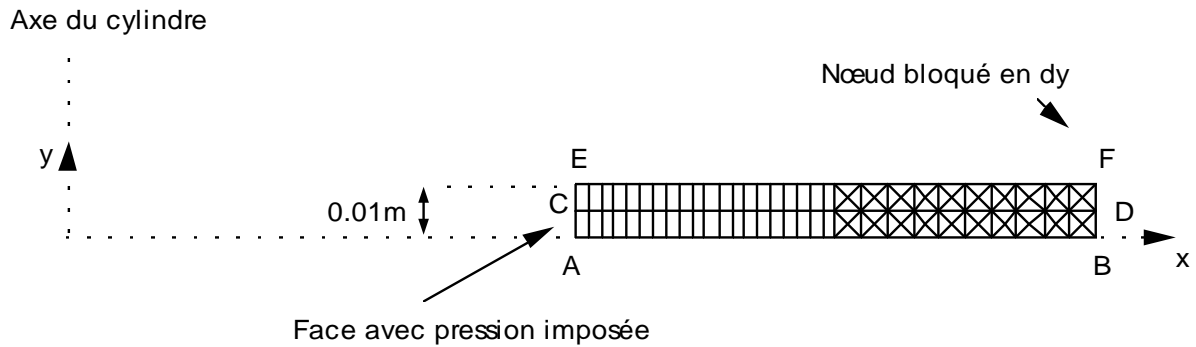
## 9.4 Quantities tested and results

Localization	Quantity	Reference	Aster	% difference
<i>A</i>	<i>u</i>	5.9 10 <sup>-5</sup>	5.9000 10 <sup>-5</sup>	0.00
	<i>v</i>	0.	eps	-
	$\sigma_{xx}$	- 60.	- 59.8354	- 0.27
	$\sigma_{vv}$	100.	99.8409	- 0.16
	$\sigma_{zz}$	0.	0.	-
	$\sigma_{xv}$	0.	0.0283	-
	$\varepsilon_{xx}$	- 4.5 10 <sup>-4</sup>	- 4.489 10 <sup>-4</sup>	- 0.24
	$\varepsilon_{vv}$	5.9 10 <sup>-4</sup>	5.890 10 <sup>-4</sup>	- 0.18
	$\varepsilon_{xv}$	0.	- 1.839 10 <sup>-7</sup>	-
<i>B</i>	<i>u</i>	4 10 <sup>-5</sup>	3.9999 10 <sup>-5</sup>	- 0.001
	<i>v</i>	0.	eps	-
	$\sigma_{xx}$	0.	-0.0189	-
	$\sigma_{vv}$	40.	40.0182	0.05
	$\sigma_{zz}$	0.	0.	-
	$\sigma_{xv}$	0.	- 3.6815 10 <sup>-3</sup>	-
	$\varepsilon_{xx}$	- 0.6 10 <sup>-4</sup>	- 0.601 10 <sup>-4</sup>	0.20
	$\varepsilon_{vv}$	2. 10 <sup>-4</sup>	2.001 10 <sup>-4</sup>	0.06
	$\varepsilon_{xv}$	0.	- 2.393 10 <sup>-8</sup>	-
<i>E</i>	<i>u</i>	4.17193 10 <sup>-5</sup>	4.17195 10 <sup>-5</sup>	0.00
	<i>v</i>	4.17193 10 <sup>-5</sup>	4.17195 10 <sup>-5</sup>	0.00
	$\sigma_{xx}$	20.	19.9745	- 0.13
	$\sigma_{vv}$	20.	20.0311	0.16
	$\sigma_{zz}$	0.	0.	-
	$\sigma_{xv}$	- 80.	- 79.8382	- 0.20
	$\varepsilon_{xx}$	0.7 10 <sup>-4</sup>	0.698 10 <sup>-4</sup>	- 0.25
	$\varepsilon_{vv}$	0.7 10 <sup>-4</sup>	0.702 10 <sup>-4</sup>	0.28
	$\varepsilon_{xv}$	- 5.2 10 <sup>-4</sup>	- 5.189 10 <sup>-4</sup>	- 0.20
<i>F</i>	<i>u</i>	2.82843 10 <sup>-5</sup>	2.82839 10 <sup>-5</sup>	- 0.001
	<i>v</i>	2.82843 10 <sup>-5</sup>	2.82839 10 <sup>-5</sup>	- 0.001
	$\sigma_{xx}$	20.	19.9960	- 0.02
	$\sigma_{vv}$	20.	20.0034	0.02
	$\sigma_{zz}$	0.	0.	-
	$\sigma_{xv}$	- 20.	- 20.0185	0.09
	$\varepsilon_{xx}$	0.7 10 <sup>-4</sup>	0.6997 10 <sup>-4</sup>	- 0.04
	$\varepsilon_{vv}$	0.7 10 <sup>-4</sup>	0.7002 10 <sup>-4</sup>	0.03
	$\varepsilon_{xv}$	- 1.3 10 <sup>-4</sup>	- 1.301 10 <sup>-4</sup>	0.09

## 10 Modelization H

### 10.1 Characteristic of the modelization

Elements AXIS (TRIA3 + QUAD4)



limiting Conditions:

node  $F$  blocked in  $dy$   
pressure on  $AE$   $p=60$ .

Names of the nodes:      $A=N111$       $B=N1$       $C=N112$   
                                $D=N3$       $E=N113$       $F=N4$

### 10.2 Characteristics of the mesh

Many nodes: 113  
Number of meshes and types: 40 QUAD4, 80 TRIA3

## 10.3 Quantities tested and results

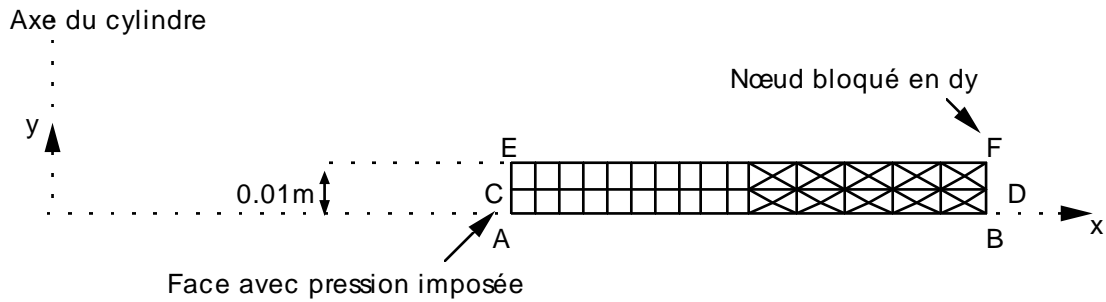
Localization	Quantity	Reference	Aster	% difference
<i>A</i>	<i>u</i>	5.9 10 <sup>-5</sup>	5.8992 10 <sup>-5</sup>	- 0.01
	<i>v</i>	0.	-	-
	$\sigma_{xx}$	- 60.	- 56.6060	- 5.66
	$\sigma_{vv}$	0.	1.0383	-
	$\sigma_{zz}$	100.	101.2924	1.29
	$\sigma_{xv}$	0.	- 1.1635	-
	$\varepsilon_{xx}$	- 4.5 10 <sup>-4</sup>	- 4.36 10 <sup>-4</sup>	- 2.99
	$\varepsilon_{vv}$	0.	- 6.18 10 <sup>-5</sup>	-
	$\varepsilon_{zz}$	5.9 10 <sup>-4</sup>	5.898 10 <sup>-4</sup>	- 0.03
	$\varepsilon_{xv}$	0.	- 1.06 10 <sup>-6</sup>	-
	<i>B</i>	<i>u</i>	4 10 <sup>-5</sup>	3.9997 10 <sup>-5</sup>
<i>v</i>		0.	-	-
$\sigma_{xx}$		0.	- 0.8951	-
$\sigma_{vv}$		0.	- 0.4106	-
$\sigma_{zz}$		40.	39.6001	- 1.00
$\sigma_{xv}$		0.	- 0.1281	-
$\varepsilon_{xx}$		- 0.6 10 <sup>-4</sup>	- 0.632 10 <sup>-4</sup>	5.43
$\varepsilon_{vv}$		0.	- 6.011 10 <sup>-5</sup>	-
$\varepsilon_{zz}$		2. 10 <sup>-4</sup>	1.999 10 <sup>-4</sup>	- 0.02
$\varepsilon_{xv}$		0.	- 8.325 10 <sup>-7</sup>	-
<i>E</i>		<i>u</i>	5.9 10 <sup>-5</sup>	5.8992 10 <sup>-5</sup>
	<i>v</i>	0.	-	-
	$\sigma_{xx}$	- 60.	- 56.6060	- 5.66
	$\sigma_{vv}$	0.	1.0383	-
	$\sigma_{zz}$	100.	101.2924	1.29
	$\sigma_{xv}$	0.	1.1635	-
	$\varepsilon_{xx}$	- 4.5 10 <sup>-4</sup>	- 4.365 10 <sup>-4</sup>	- 2.99
	$\varepsilon_{vv}$	0.	- 6.184 10 <sup>-5</sup>	-
	$\varepsilon_{zz}$	5.9 10 <sup>-4</sup>	5.898 10 <sup>-4</sup>	- 0.03
	$\varepsilon_{xv}$	0.	1.063 10 <sup>-6</sup>	-
	<i>F</i>	<i>u</i>	4 10 <sup>-5</sup>	3.9997 10 <sup>-5</sup>
<i>v</i>		0.	-	-
$\sigma_{xx}$		0.	- 0.4221	-
$\sigma_{vv}$		0.	- 0.2280	-
$\sigma_{zz}$		40.	39.8015	- 0.50
$\sigma_{xv}$		0.	- 0.0020	-
$\varepsilon_{xx}$		- 0.6 10 <sup>-4</sup>	- 0.615 10 <sup>-4</sup>	2.45
$\varepsilon_{vv}$		0.	- 6.021 10 <sup>-5</sup>	-
$\varepsilon_{zz}$		2. 10 <sup>-4</sup>	1.9998 10 <sup>-4</sup>	- 0.01
$\varepsilon_{xv}$		0.	- 1.280 10 <sup>-8</sup>	-



## 11 Modelization I

### 11.1 Characteristic of the modelization

Elements **AXIS** (TRIA6 + QUAD8)



limiting Conditions:

Node  $F$  blocked in  $dy$   
pressure on  $AE$   $p=60$ .

Names of the nodes:       $A=N8$                $B=N174$                $C=N5$   
                                  $D=N170$                $E=N3$                  $F=N159$

### 11.2 Characteristics of the mesh

Many nodes: 175  
Number of meshes and types: 20 QUAD8, 40 TRIA6

## 11.3 Quantities tested and results

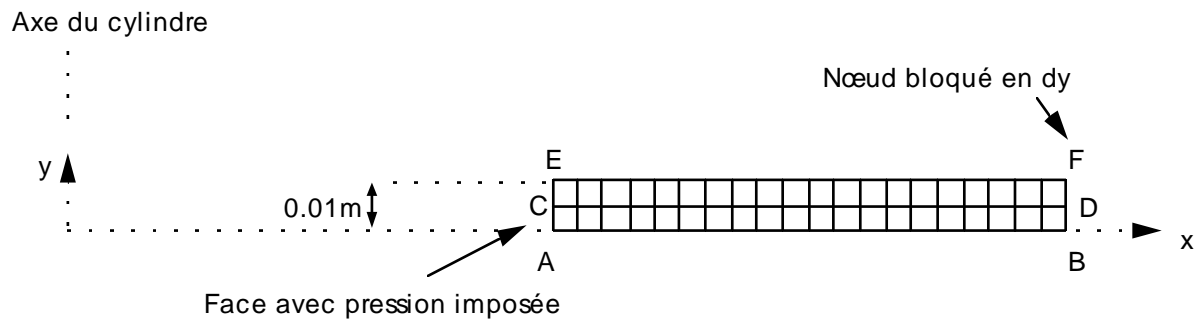
Localization	Quantity	Reference	Aster	% difference
<i>A</i>	<i>u</i>	5.9 10 <sup>-5</sup>	5.9000 10 <sup>-5</sup>	0.00
	<i>v</i>	0.	-	-
	$\sigma_{xx}$	- 60.	- 59.8976	- 0.17
	$\sigma_{yy}$	0.	- 0.0024	-
	$\sigma_{zz}$	100.	99.9089	- 0.09
	$\sigma_{xy}$	0.	- 0.0137	-
	$\epsilon_{xx}$	- 4.5 10 <sup>-4</sup>	- 4.493 10 <sup>-4</sup>	- 0.14
	$\epsilon_{yy}$	0.	- 6.003 10 <sup>-5</sup>	-
	$\epsilon_{zz}$	5.9 10 <sup>-4</sup>	5.894 10 <sup>-4</sup>	- 0.10
	$\epsilon_{xy}$	0.	- 8.895 10 <sup>-8</sup>	-
<i>B</i>	<i>u</i>	4 10 <sup>-5</sup>	4.0000 10 <sup>-5</sup>	0.00
	<i>v</i>	0.	-	-
	$\sigma_{xx}$	0.	0.0308	-
	$\sigma_{yy}$	0.	- 0.0020	-
	$\sigma_{zz}$	40.	39.9738	- 0.07
	$\sigma_{xy}$	0.	0.0131	-
	$\epsilon_{xx}$	- 0.6 10 <sup>-4</sup>	- 0.598 10 <sup>-4</sup>	- 0.33
	$\epsilon_{yy}$	0.	- 6.002 10 <sup>-5</sup>	-
	$\epsilon_{zz}$	2. 10 <sup>-4</sup>	1.998 10 <sup>-4</sup>	- 0.09
	$\epsilon_{xy}$	0.	8.495 10 <sup>-8</sup>	-
<i>E</i>	<i>u</i>	5.9 10 <sup>-5</sup>	5.9000 10 <sup>-5</sup>	0.00
	<i>v</i>	0.	-	-
	$\sigma_{xx}$	- 60.	- 59.8976	- 0.17
	$\sigma_{yy}$	0.	- 0.0024	-
	$\sigma_{zz}$	100.	99.9089	- 0.09
	$\sigma_{xy}$	0.	0.0137	-
	$\epsilon_{xx}$	- 4.5 10 <sup>-4</sup>	- 4.493 10 <sup>-4</sup>	- 0.14
	$\epsilon_{yy}$	0.	- 6.003 10 <sup>-5</sup>	-
	$\epsilon_{zz}$	5.9 10 <sup>-4</sup>	5.894 10 <sup>-4</sup>	- 0.10
	$\epsilon_{xy}$	0.	8.895 10 <sup>-8</sup>	-
<i>F</i>	<i>u</i>	4 10 <sup>-5</sup>	4.0000 10 <sup>-5</sup>	0.00
	<i>v</i>	0.	-	-
	$\sigma_{xx}$	0.	0.0308	-
	$\sigma_{yy}$	0.	- 0.0020	-
	$\sigma_{zz}$	40.	39.9738	- 0.07
	$\sigma_{xy}$	0.	- 0.0131	-
	$\epsilon_{xx}$	- 0.6 10 <sup>-4</sup>	- 0.598 10 <sup>-4</sup>	- 0.33
	$\epsilon_{yy}$	0.	- 6.002 10 <sup>-5</sup>	-
	$\epsilon_{zz}$	2. 10 <sup>-4</sup>	1.998 10 <sup>-4</sup>	- 0.09
	$\epsilon_{xy}$	0.	- 8.495 10 <sup>-8</sup>	it

has compared to the end of this test a loading in rotation into axisymmetric pure with the same loading as a Fourier mode 0. One finds many identical results.

## 12 Modelization J

### 12.1 Characteristic of the modelization

Elements **AXIS** (QUAD9)



limiting Conditions:

node  $F$  blocked in  $dy$   
pressure on  $AE$   $p=60$ .

Names of the nodes:       $A=N196$        $B=N1$        $C=N200$   
                                  $D=N5$        $E=N202$        $F=N7$

### 12.2 Characteristics of the mesh

Many nodes: 205  
Number of meshes and types: 40 QUAD9

## 12.3 Quantities tested and results

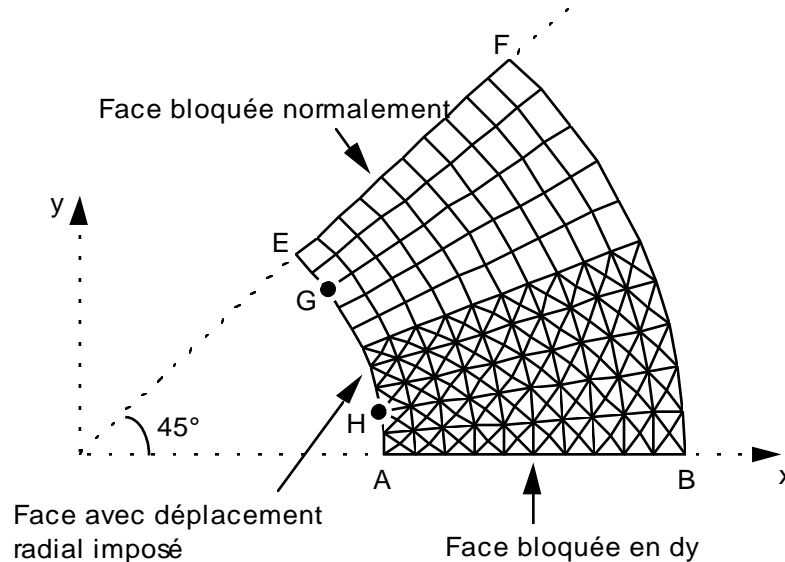
Localization	Quantity	Reference	Aster	% difference
<i>A</i>	<i>u</i>	5.9 10 <sup>-5</sup>	5.9000 10 <sup>-5</sup>	0.00
	<i>v</i>	0.	-	-
	$\sigma_{xx}$	- 60.	- 59.8997	- 0.17
	$\sigma_{vv}$	0.	- 0.0035	-
	$\sigma_{zz}$	100.	99.9080	- 0.09
	$\sigma_{xv}$	0.	- 0.0141	-
	$\epsilon_{xx}$	- 4.5 10 <sup>-4</sup>	- 4.494 10 <sup>-4</sup>	- 0.14
	$\epsilon_{vv}$	0.	- 6.003 10 <sup>-5</sup>	-
	$\epsilon_{zz}$	5.9 10 <sup>-4</sup>	5.894 10 <sup>-4</sup>	- 0.10
	$\epsilon_{xv}$	0.	- 9.156 10 <sup>-8</sup>	-
	<i>B</i>	<i>u</i>	4. 10 <sup>-5</sup>	4.0000 10 <sup>-5</sup>
<i>v</i>		0.	-	-
$\sigma_{xx}$		0.	0.0070	-
$\sigma_{vv}$		0.	- 0.0001	-
$\sigma_{zz}$		40.	39.9936	- 0.02
$\sigma_{xv}$		0.	0.0010	-
$\epsilon_{xx}$		- 0.6 10 <sup>-4</sup>	- 0.5996 10 <sup>-4</sup>	- 0.07
$\epsilon_{vv}$		0.	- 6.000 10 <sup>-5</sup>	-
$\epsilon_{zz}$		2. 10 <sup>-4</sup>	1.9996 10 <sup>-4</sup>	- 0.02
$\epsilon_{xv}$		0.	6.748 10 <sup>-9</sup>	-
<i>E</i>		<i>u</i>	5.9 10 <sup>-5</sup>	5.9000 10 <sup>-5</sup>
	<i>v</i>	0.	-	-
	$\sigma_{xx}$	- 60.	- 59.8997	- 0.17
	$\sigma_{vv}$	0.	- 0.0035	-
	$\sigma_{zz}$	100.	99.9080	- 0.09
	$\sigma_{xv}$	0.	0.0141	-
	$\epsilon_{xx}$	- 4.5 10 <sup>-4</sup>	- 4.494 10 <sup>-4</sup>	- 0.14
	$\epsilon_{vv}$	0.	- 6.003 10 <sup>-5</sup>	-
	$\epsilon_{zz}$	5.9 10 <sup>-4</sup>	5.894 10 <sup>-4</sup>	- 0.10
	$\epsilon_{xv}$	0.	- 9.156 10 <sup>-8</sup>	-
	<i>F</i>	<i>u</i>	4. 10 <sup>-5</sup>	4.0000 10 <sup>-5</sup>
<i>v</i>		0.	-	-
$\sigma_{xx}$		0.	0.0070	-
$\sigma_{vv}$		0.	- 0.0001	-
$\sigma_{zz}$		40.	39.9936	- 0.02
$\sigma_{xv}$		0.	- 0.0010	-
$\epsilon_{xx}$		- 0.6 10 <sup>-4</sup>	- 0.5996 10 <sup>-4</sup>	- 0.07
$\epsilon_{vv}$		0.	- 6.000 10 <sup>-5</sup>	-
$\epsilon_{zz}$		2. 10 <sup>-4</sup>	1.9996 10 <sup>-4</sup>	- 0.02
$\epsilon_{xv}$		0.	- 6.748 10 <sup>-9</sup>	-

## 13 Modelization K

### 13.1 Characteristic of the modelization

Elements 3D (PENTA6 and HEXA8)

Mesh obtained by extrusion starting from the mesh 2D below (modelization E)



Along the axis  $Z$  : 2 layers of elements  
total Thickness: 0.01m

Limiting conditions:

the node is outside the field of definition with a right profile of the EXCLU type node:  $F \quad u_z = 0$

face  $AB$  blocked opposite  $dy$

$EF$  blocked normally

face  $AE$  radial displacement imposed on  $5.9 E - 5 m$

Names the nodes:	$A = No1$	$C = No36$	$D = No166$
plane $z = 0.005$	$A2 = No172$	$C2 = No242$	$D2 = No5025$
plane $z = 0.01$	$A3 = No173$	$C3 = No243$	$D3 = No503$

Names of the nodes:	$E = No41$	$H = No9$	$G = No38$
plane $z = 0.005$	$E2 = No252$	$H2 = No188$	$G2 = No246$
plane $z = 0.01$	$E3 = No253$	$H3 = No189$	$G3 = No247$

### 13.2 Characteristics of the mesh

Many nodes: 513

Number of meshes and types: 400 PENTA6, 100 HEXA8 40 QUAD4 (sides skin interns)

### 13.3 Remarks

the loading are here in imposed displacement, contrary to the other modelizations. The reactions are tested.

Warning : The translation process used on this website is a "Machine Translation". It may be imprecise and inaccurate in whole or in part and is provided as a convenience.

## 13.4 Quantities tested and results

Localization	Quantity	Reference	Aster	% difference
$C$	$F_x$	1.0884 E-3	1.0953 E-3	0.64
	$F_y$	4.5084 E-4	4.5836 E-4	1.67
$C_2$	$F_x$	2.1768 E-3	2.1571 E-3	- 0.91
	$F_y$	9.0170 E-4	9.1304 E-4	1.26
$C_3$	$F_x$	1.0884 E-3	1.0953 E-3	0.64
	$F_y$	4.5084 E-4	4.5836 E-4	1.67
$H$	$F_x$	1.1636 E-3	1.1709 E-3	0.63
	$F_y$	1.8429 E-4	1.8527 E-4	0.53
$G$	$F_x$	1.0045 E-3	1.0144 E-3	0.99
	$F_y$	6.1550 E-4	6.2117 E-4	0.92
$H_2$	$F_x$	2.3272 E-3	2.3173 E-3	- 0.43
	$F_y$	3.6858 E-4	3.6669 E-4	- 0.51
$G_2$	$F_x$	2.0090 E-3	1.9951 E-3	- 0.69
	$F_y$	1.2310 E-3	1.2214 E-3	- 0.78

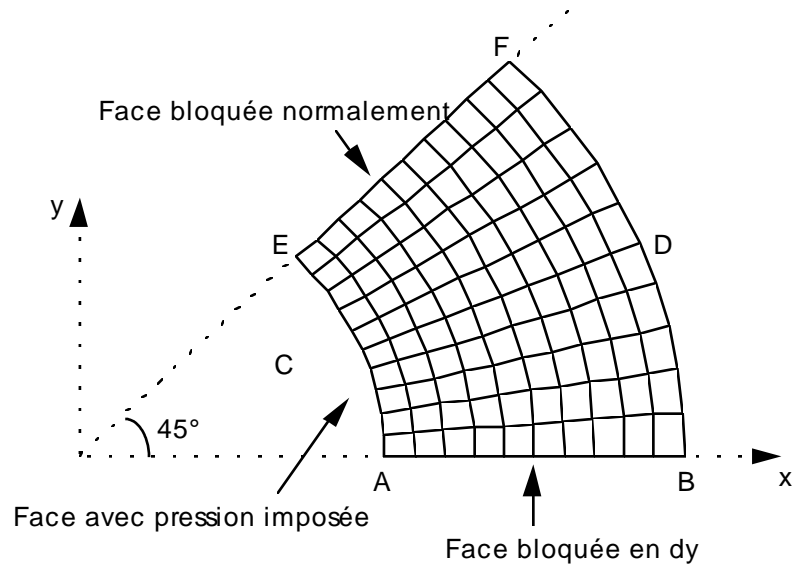
## 13.5 Remarks

It is checked that the nodal forces of reactions are null in all the nodes, except on the nodes of surface  $AE$  and surfaces  $EF$  and  $AB$ .

## 14 Modelization L

### 14.1 Characteristic of the modelization

Elements 3D (PYRAM5)



Along the axis  $Z$  : each parallelepiped is cut out in 6 pyramids  
total Thickness: 0.01m

Limiting conditions:

the node is outside the field of definition with a right profile of the EXCLU type  
node:  $F \quad u_z=0$

face  $AB$  blocked opposite  $dy$

$EF$  blocked normally

pressure on the face  $AE \quad p=60.$

Names the nodes:  $A=N267 \quad B=N142 \quad E=N29 \quad F=N1$

### 14.2 Characteristics of the mesh

Many nodes: 342

Number of meshes and types: 600 PYRAM5 620 QUAD4 (sides skin interns)

### 14.3

## 14.4 Quantities tested and results

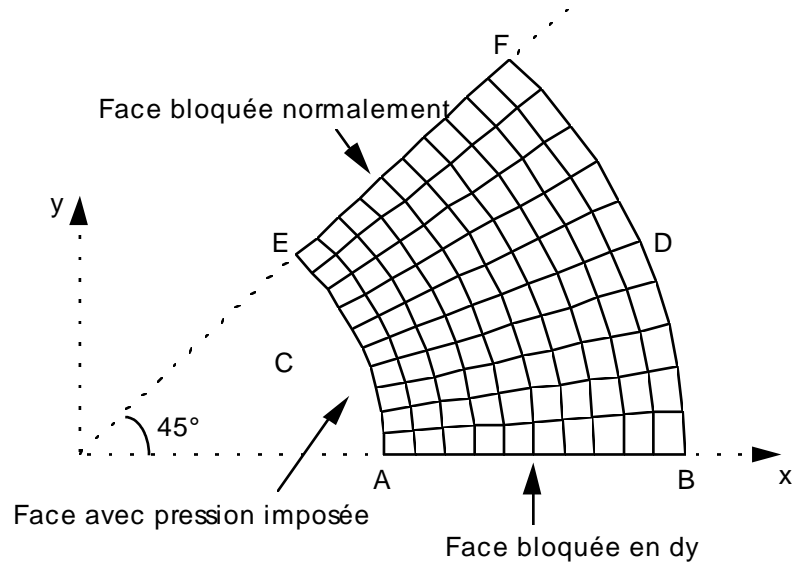
Identification	Reference	Aster	% difference
$u$ - node (A)	$5.9 \cdot 10^{-5}$	$5.8873 \cdot 10^{-5}$	- 0.21
$v$ - node (A)	0.	eps	-
$\sigma_{xx}$ - node (A)	- 60.	- 52.9567	- 11.74
$\sigma_{vv}$ - node (A)	100.	91.7830	- 8.22
$\sigma_{zz}$ - node (A)	0.	- 1.1206	-
$\sigma_{xv}$ - node (A)	0.	- 4.5121	-
$\varepsilon_{xx}$ - node (A)	- $4.5 \cdot 10^{-4}$	- $4.008 \cdot 10^{-4}$	- 10.94
$\varepsilon_{vv}$ - node (A)	$5.9 \cdot 10^{-4}$	$5.400 \cdot 10^{-4}$	- 8.47
$\varepsilon_{xv}$ - node (A)	0.	- $2.933 \cdot 10^{-5}$	-
$u$ - node (B)	$4. \cdot 10^{-5}$	$3.9936 \cdot 10^{-5}$	- 0.16
$v$ - node (B)	0.	eps	-
$\sigma_{xx}$ - node (B)	0.	- 0.7670	-
$\sigma_{vv}$ - node (B)	40.	39.5319	- 1.17
$\sigma_{zz}$ - node (B)	0.	- 0.3115	-
$\sigma_{xv}$ - node (B)	0.	- 1.5858	-
$\varepsilon_{xx}$ - node (B)	- $0.6 \cdot 10^{-4}$	- $0.627 \cdot 10^{-4}$	4.44
$\varepsilon_{vv}$ - node (B)	$2. \cdot 10^{-4}$	$1.993 \cdot 10^{-4}$	- 0.36
$\varepsilon_{xv}$ - node (B)	0.	- $1.031 \cdot 10^{-5}$	-
$u$ - node (E)	$4.17193 \cdot 10^{-5}$	$4.16293 \cdot 10^{-5}$	- 0.21
$v$ - node (E)	$4.17193 \cdot 10^{-5}$	$4.16293 \cdot 10^{-5}$	- 0.21
$\sigma_{xx}$ - node (E)	20.	19.3586	- 3.21
$\sigma_{vv}$ - node (E)	20.	31.5151	57.57
$\sigma_{zz}$ - node (E)	0.	2.5686	-
$\sigma_{xv}$ - node (E)	- 80.	- 77.2309	- 3.46
$\varepsilon_{xx}$ - node (E)	$0.7 \cdot 10^{-4}$	$0.457 \cdot 10^{-4}$	- 34.76
$\varepsilon_{vv}$ - node (E)	$0.7 \cdot 10^{-4}$	$1.247 \cdot 10^{-4}$	78.12
$\varepsilon_{xv}$ - node (E)	- $5.2 \cdot 10^{-4}$	- $5.020 \cdot 10^{-4}$	- 3.46
$u$ - node (F)	$2.82843 \cdot 10^{-5}$	$2.82393 \cdot 10^{-5}$	- 0.16
$v$ - node (F)	$2.82843 \cdot 10^{-5}$	$2.82393 \cdot 10^{-5}$	- 0.16
$\sigma_{xx}$ - node (F)	20.	18.9523	- 5.24
$\sigma_{vv}$ - node (F)	20.	20.9510	4.75
$\sigma_{zz}$ - node (F)	0.	0.0035	-
$\sigma_{xv}$ - node (F)	- 20.	- 20.9897	4.95
$\varepsilon_{xx}$ - node (F)	$0.7 \cdot 10^{-4}$	$0.633 \cdot 10^{-4}$	- 9.60
$\varepsilon_{vv}$ - node (F)	$0.7 \cdot 10^{-4}$	$0.763 \cdot 10^{-4}$	8.96
$\varepsilon_{xv}$ - node (F)	- $1.3 \cdot 10^{-4}$	- $1.364 \cdot 10^{-4}$	4.95



## 15 Modelization M

### 15.1 Characteristic of the modelization

Elements 3D (PYRAM13)



Along the axis  $Z$  : each parallelepiped is cut out in 6 pyramids  
total Thickness: 0.01m

Limiting conditions:

the node is outside the field of definition with a right profile of the EXCLU type node:  $F \quad u_z=0$

face  $AB$  blocked opposite  $dy$

$EF$  blocked normally

pressure on the face  $AE \quad p=60.$

Names the nodes:  $A=N1403 \quad B=N734 \quad E=N152 \quad F=N4$

### 15.2 Characteristics of the mesh

Many nodes: 1703

Number of meshes and types: 600 PYRAM13 620 QUAD8 (sides skin interns)

### 15.3

## 15.4 Quantities tested and results

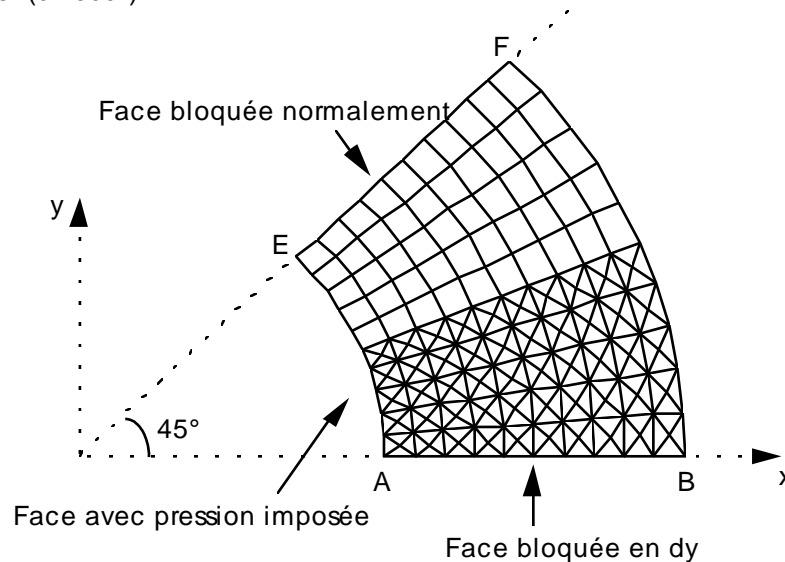
Identification	Reference	Aster	% difference
$u$ - node (A)	$5.9 \cdot 10^{-5}$	$5.8999 \cdot 10^{-5}$	-0.002
$v$ - node (A)	0.	eps	-
$\sigma_{xx}$ - node (A)	-60.	-59.9880	-0.02
$\sigma_{vv}$ - node (A)	100.	100.1277	0.13
$\sigma_{zz}$ - node (A)	0.	0.0425	-
$\sigma_{xv}$ - node (A)	0.	-0.0913	-
$\varepsilon_{xx}$ - node (A)	$-4.5 \cdot 10^{-4}$	$-4.502 \cdot 10^{-4}$	0.04
$\varepsilon_{vv}$ - node (A)	$5.9 \cdot 10^{-4}$	$5.906 \cdot 10^{-4}$	0.09
$\varepsilon_{xv}$ - node (A)	0.	$-5.934 \cdot 10^{-7}$	-
$u$ - node (B)	$4. \cdot 10^{-5}$	$4.0000 \cdot 10^{-5}$	0.00
$v$ - node (B)	0.	eps	-
$\sigma_{xx}$ - node (B)	0.	-0.0276	-
$\sigma_{vv}$ - node (B)	40.	40.0331	0.08
$\sigma_{zz}$ - node (B)	0.	0.0024	-
$\sigma_{xv}$ - node (B)	0.	0.0126	-
$\varepsilon_{xx}$ - node (B)	$-0.6 \cdot 10^{-4}$	$-0.602 \cdot 10^{-4}$	0.32
$\varepsilon_{vv}$ - node (B)	$2. \cdot 10^{-4}$	$2.002 \cdot 10^{-4}$	0.10
$\varepsilon_{xv}$ - node (B)	0.	$8.177 \cdot 10^{-8}$	-
$u$ - node (E)	$4.17193 \cdot 10^{-5}$	$4.17183 \cdot 10^{-5}$	-0.002
$v$ - node (E)	$4.17193 \cdot 10^{-5}$	$4.17183 \cdot 10^{-5}$	-0.002
$\sigma_{xx}$ - node (E)	20.	19.9787	-0.11
$\sigma_{vv}$ - node (E)	20.	20.1612	0.81
$\sigma_{zz}$ - node (E)	0.	0.0425	-
$\sigma_{xv}$ - node (E)	-80.	-80.0580	0.07
$\varepsilon_{xx}$ - node (E)	$0.7 \cdot 10^{-4}$	$0.696 \cdot 10^{-4}$	-0.59
$\varepsilon_{vv}$ - node (E)	$0.7 \cdot 10^{-4}$	$0.708 \cdot 10^{-4}$	1.11
$\varepsilon_{xv}$ - node (E)	$-5.2 \cdot 10^{-4}$	$-5.204 \cdot 10^{-4}$	0.07
$u$ - node (F)	$2.82843 \cdot 10^{-5}$	$2.82844 \cdot 10^{-5}$	0.00
$v$ - node (F)	$2.82843 \cdot 10^{-5}$	$2.82844 \cdot 10^{-5}$	0.00
$\sigma_{xx}$ - node (F)	20.	20.0224	0.11
$\sigma_{vv}$ - node (F)	20.	19.9901	-0.05
$\sigma_{zz}$ - node (F)	0.	0.0031	-
$\sigma_{xv}$ - node (F)	-20.	-19.9818	-0.09
$\varepsilon_{xx}$ - node (F)	$0.7 \cdot 10^{-4}$	$0.701 \cdot 10^{-5}$	0.17
$\varepsilon_{vv}$ - node (F)	$0.7 \cdot 10^{-4}$	$0.699 \cdot 10^{-4}$	-0.13
$\varepsilon_{xv}$ - node (F)	$-1.3 \cdot 10^{-5}$	$-1.299 \cdot 10^{-5}$	-0.09

## 16 Modelization N

### 16.1 Characteristic of the modelization

#### Elements 3D (PENTA15 and HEXA20)

Mesh obtained by extrusion from a mesh 2D resembling the mesh below (8 elements in the radial direction, 4+4 elements in the direction circumferential) and duplicated to have a complete section of the cylinder (on 360°).



Along the axis  $Z$  : 1 layer of elements  
total Thickness: 0.01m

Limiting conditions:

face  $AB$  blocked opposite  $dy$   
 $EF$  blocked normally

pressure on the face  $AE$   $p=60$ .  
basic effect on the sections  $p=60$ .

Names of the nodes:  $A=N5349$        $B=N6092$        $C=N433$   
 $D=N441$        $E=N2180$        $F=N1632$

### 16.2 Characteristics of the mesh

Many nodes: 8832  
Number of meshes and types: 1024 PENTA15, 512 HEXA20, 1176 QUAD8 and 2048 TRIA6.

### 16.3 Remarks

Contrary to the preceding modelizations, one takes into account here the basic effect applying to the sections at the ends of the cylinder.

### 16.4

## 16.5 Quantities tested and results

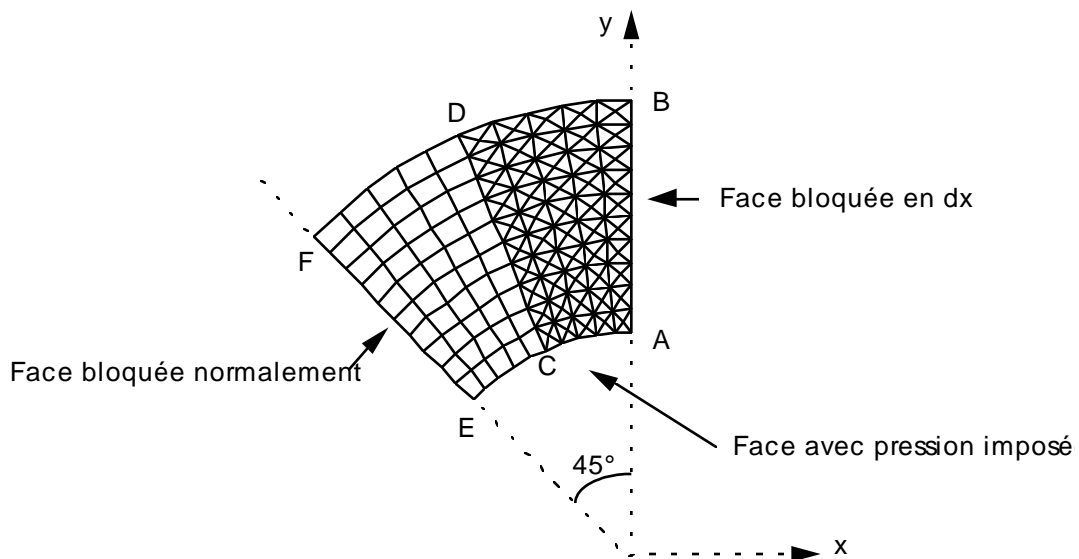
Identification	Reference	Aster	% difference
$u$ - node (A)	$5.6 \cdot 10^{-5}$	$5.6000 \cdot 10^{-5}$	0.00
$\nu$ - node (A)	0.	eps	-
$\sigma_{xx}$ - node (A)	- 60.	-59.5972	- 0.67
$\sigma_{\nu\nu}$ - node (A)	100.	99.5187	- 0.48
$\sigma_{zz}$ - node (A)	20.	19.9584	- 0.21
$\sigma_{x\nu}$ - node (A)	0.	eps	-
$u$ - node (B)	$3.4 \cdot 10^{-5}$	$3.4000 \cdot 10^{-5}$	0.00
$\nu$ - node (B)	0.	eps	-
$\sigma_{xx}$ - node (B)	0.	$2.0877 \cdot 10^{-2}$	-
$\sigma_{\nu\nu}$ - node (B)	40.	39.9685	- 0.08
$\sigma_{zz}$ - node (B)	20.	19.9946	- 0.03
$\sigma_{x\nu}$ - node (B)	0.	eps	-
$\sigma_{xx}$ - node (E)	20.	20.3287	1.64
$\sigma_{\nu\nu}$ - node (E)	20.	20.3287	1.64
$\sigma_{zz}$ - node (E)	20.	20.1739	0.87
$\sigma_{x\nu}$ - node (E)	- 80.	-79.9775	- 0.03
$\sigma_{xx}$ - node (F)	20.	20.0176	0.09
$\sigma_{\nu\nu}$ - node (F)	20.	20.0176	0.09
$\sigma_{zz}$ - node (F)	20.	20.0072	0.04
$\sigma_{x\nu}$ - node (F)	- 20.	-20.0027	0.01

## 17 Modelization O

### 17.1 Characteristic of the modelization

Elements `C_PLAN` (QUAD8 + TRIA6)

Mesh 2D resembling the mesh below (8 elements in the radial direction, 4+4 elements in the direction circumferential) and duplicated to have a complete section of the cylinder (on 360°).



Limiting conditions:

side  $AB$  blocked in  $dx$   
side  $EF$  normally blocked  
pressure on  $AE$   $p=60$ .

Names of the nodes:       $A=N249$                $B=N992$                $C=N1667$   
                                  $D=N1588$                $E=N3776$                $F=N3228$

### 17.2 Characteristics of the mesh

Many nodes: 3840  
Number of meshes and types: 1026 TRIA6, 512 QUAD8

### 17.3

## 17.4 Quantities tested and results

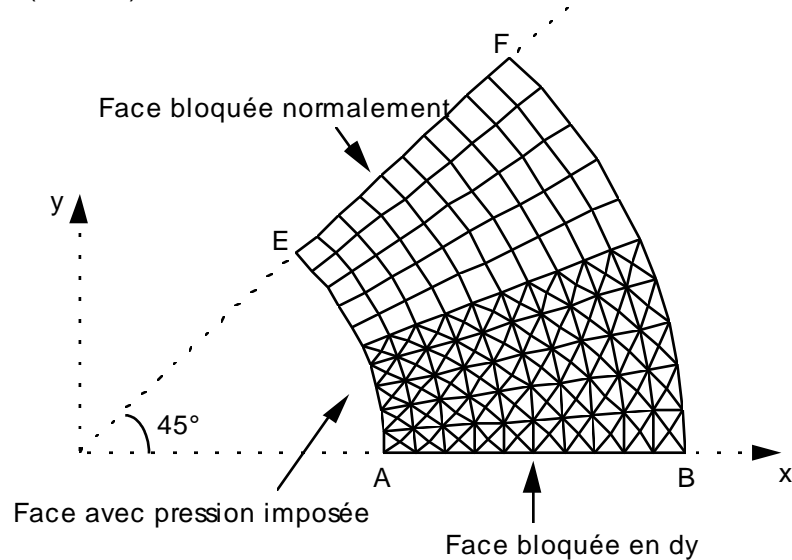
Identification	Reference	Aster	% difference
$u$ - node (A)	$5.9 \cdot 10^{-5}$	$5.8999 \cdot 10^{-5}$	-0.002
$v$ - node (A)	0.	eps	-
$\sigma_{xx}$ - node (A)	-60.	-59.5340	-0.78
$\sigma_{yy}$ - node (A)	100.	99.5453	-0.45
$\sigma_{zz}$ - node (A)	0.	0.	-
$\sigma_{xy}$ - node (A)	0.	eps	-
$u$ - node (B)	$4. \cdot 10^{-5}$	$3.99996 \cdot 10^{-5}$	0.00
$v$ - node (B)	0.	0.	-
$\sigma_{xx}$ - node (B)	0.	$2.6874 \cdot 10^{-2}$	-
$\sigma_{yy}$ - node (B)	40.	39.9716	-0.07
$\sigma_{zz}$ - node (B)	0.	0.	-
$\sigma_{xy}$ - node (B)	0.	eps	-
$u$ - node (E)	$4.17193 \cdot 10^{-5}$	$4.17215 \cdot 10^{-5}$	0.005
$v$ - node (E)	$4.17193 \cdot 10^{-5}$	$4.17215 \cdot 10^{-5}$	0.005
$\sigma_{xx}$ - node (E)	20.	20.2875	1.44
$\sigma_{yy}$ - node (E)	20.	20.2875	1.44
$\sigma_{zz}$ - node (E)	0.	0.	-
$\sigma_{xy}$ - node (E)	-80.	-79.9196	-0.10
$u$ - node (F)	$2.82843 \cdot 10^{-5}$	$2.82841 \cdot 10^{-5}$	-0.001
$v$ - node (F)	$2.82843 \cdot 10^{-5}$	$2.82841 \cdot 10^{-5}$	-0.001
$\sigma_{xx}$ - node (F)	20.	20.0167	0.08
$\sigma_{yy}$ - node (F)	20.	20.0167	0.08
$\sigma_{zz}$ - node (F)	0.	0.	-
$\sigma_{xy}$ - node (F)	-20.	-19.9993	-0.004

## 18 Modelization P

### 18.1 Characteristic of the modelization

#### Elements 3D (PENTA15 and HEXA20) – even mesh that the modelization N

Mesh obtained by extrusion from a mesh 2D resembling the mesh below (8 elements in the radial direction, 4+4 elements in the direction circumferential) and duplicated to have a complete section of the cylinder (on 360°).



Along the axis  $Z$  : 1 layer of elements  
total Thickness: 0.01m

Limiting conditions:

normally  $EF$  blocked face  
face  $AB$  blocked in  $dy$   
pressure on the face  $AE$   $f_p$   
basic effect on the sections  $f_p$

With  $f_p$  : linear pressure function of time being worth 60. with  $t=1s$  and 120.  $t=2s$

Names of the nodes:  $A=N5349$   $B=N6092$   $C=N433$   
 $D=N441$   $E=N2180$   $F=N1632$

### 18.2 Characteristics of the mesh

Many nodes: 8832

Number of meshes and types: 1024 PENTA15, 512 HEXA20, 1176 QUAD8 and 2048 TRIA6.

### 18.3 Remarks

Contrary to the modelization N, one tests here a basic pressure and effect variables according to time. A linear variation of the pressure involves a linear variation of the stresses.

### 18.4

## 18.5 Quantities tested and results

Identification	Reference	Aster	% difference
U-node (A) to t=1. S	5.6 10-5	5.6000 10-5	0.00
V-node (A) with t=1. S	0.	eps	-
$\sigma_{xx}$ - node (A) with t=1. S	- 60.	-59.5414	- 0.76
$\sigma_{vv}$ - node (A) with t=1. S	100.	99.6183	- 0.38
$\sigma_{zz}$ - node (A) with t=1. S	20.	19.9976	- 0.01
$\sigma_{xv}$ - node (A) with t=1. S	0.	eps	-
$\sigma_{xx}$ - node (A) with t=2. S	- 120.	-119.0829	- 0.76
$\sigma_{vv}$ - node (A) with t=2. S	200.	199.2366	- 0.38
$\sigma_{zz}$ - node (A) with t=2. S	40.	39.9952	- 0.01
$\sigma_{xv}$ - node (A) with t=2. S	0.	eps	-
U-node (B) with t=1. S	3.4 10-5	3.4000 10-5	0.00
V-node (B) with t=1. S	0.	eps	-
$\sigma_{xx}$ - node (B) with t=1. S	0.	2.6761 10-2	-
$\sigma_{vv}$ - node (B) with t=1. S	40.	39.9740	- 0.06
$\sigma_{zz}$ - node (B) with t=1. S	20.	19.9973	- 0.01
$\sigma_{xv}$ - node (B) with t=1. S	0.	eps	-
$\sigma_{xx}$ - node (B) with t=2. S	0.	5.3523 10-2	-
$\sigma_{vv}$ - node (B) with t=2. S	80.	79.9480	- 0.06
$\sigma_{zz}$ - node (B) with t=2. S	40.	39.9946	- 0.01
$\sigma_{xv}$ - node (B) with t=2. S	0.	eps	-
$\sigma_{xx}$ - node (E) with t=1. S	20.	20.3287	1.64
$\sigma_{vv}$ - node (E) with t=1. S	20.	20.3287	1.64
$\sigma_{zz}$ - node (E) with t=1. S	20.	20.1739	0.87
$\sigma_{xv}$ - node (E) with t=1. S	- 80.	-79.9775	- 0.03
$\sigma_{xx}$ - node (E) with t=2. S	40.	40.6575	1.64
$\sigma_{vv}$ - node (E) with t=2. S	40.	40.6575	1.64
$\sigma_{zz}$ - node (E) with t=2. S	40.	40.3479	0.87
$\sigma_{xv}$ - node (E) with t=2. S	- 160.	-159.9550	- 0.03
$\sigma_{xx}$ - node (F) with t=1. S	20.	20.0176	0.09
$\sigma_{vv}$ - node (F) with t=1. S	20.	20.0176	0.09
$\sigma_{zz}$ - node (F) with t=1. S	20.	20.0072	0.04
$\sigma_{xv}$ - node (F) with t=1. S	- 20.	-20.0027	0.01
$\sigma_{xx}$ - node (F) with t=2. S	40.	40.0351	0.09
$\sigma_{vv}$ - node (F) with t=2. S	40.	40.0351	0.09
$\sigma_{zz}$ - node (F) with t=2. S	40.	40.0144	0.04
$\sigma_{xv}$ - node (F) with t=2. S	- 40.	-40.0054	0.01



## 19 Summary of the Summary

results of the errors max in %

3D	Localization	MOD A	MOD B	MOD C	MOD D	MOD L	MOD M	MOD N	MOD P
elem		pe6, h8	pe15, h20	te4	te10	py5	py13	pe15, h20	pe15, h20
geom		45°	45°	45°	45°	45°	45°	360°	360°
Nb		1922	2115	1115	1395	342	1703	8832	8832
No									
Dépl.	A, E	0.08	0.09	0.17	0.04	0.21	0.00	0.00	0.00
	B, F	0.10	0.07	0.30	0.04	0.16	0.00	0.00	0.00
$\sigma_{xx}$	A, E	4.59	0.39	10.45	4.41	11.74	0.11	1.64	1.64
	B, F	5.24	0.07	7.78	0.95	5.24	0.11	0.09	0.09
$\sigma_{yy}$	A, E	5.70	0.92	9.46	1.80	57.57	0.81	1.64	1.64
	B, F	1.89	0.01	2.46	0.49	4.75	0.08	0.09	0.09
$\sigma_{zz}$	A, E	Good	Good	Good	Good	Good	Good	0.87	0.87
	B, F	Good	Good	Good	Good	Good	Good	0.04	0.04
$\sigma_{xy}$	A, E	0.15	0.26	2.89	0.27	3.46	0.07	0.03	0.03
	B, F	0.90	0.06	0.81	0.28	4.95	0.09	0.01	0.01

C_PLAN	Localization	MOD E	MOD F	MOD G	MOD O
Type of elements		tria3, quad4	tria6, quad8	quad9	tria6, quad8
modelled Geometry		45°	45°	45°	360°
Many nodes		961.591.441			384
Displacements	A, E	0.07	0.09	0.00	0.01
	B, F	0.09	0.07	0.00	0.00
Stresses $\sigma_{xx}$	A, E	4.65	0.39	0.27	1.44
	B, F	5.19	0.06	0.02	0.08
Stresses $\sigma_{yy}$	A, E	5.68	0.90	0.16	1.44
	B, F	1.40	0.04	0.05	0.08
Stresses $\sigma_{zz}$	A, E	Good	Good	Good	Good
	B, F	Good	Good	Good	Good
Stresses $\sigma_{xy}$	A, E	0.16	0.23	0.20	0.10
	B, F	1.23	0.07	0.09	0.00

AXIS	Localization	MOD H	MOD I	MOD J
Standard of elements		tria3, quad4	tria6, quad8	quad9
Many nodes		113.175.205		
Displacements	A, E	0.01	0.00	0.00
	B, F	0.01	0.00	0.00
Stresses $\sigma_{xx}$	A, E	5.66	0.17	0.17
	B, F	Good	Good	Good
Stresses $\sigma_{yy}$	A, E	Good	Good	Good
	B, F	Good	Good	Good
Stresses $\sigma_{zz}$	A, E	1.29	0.09	0.09
	B, F	1.00	0.07	0.02
Stresses $\sigma_{xy}$	A, E	the Good	Good	Good
	B, F	Good	Good	Good

- results are more precise with elements of order 2.
- The problem is adapted more to an axisymmetric modelization. The results are better.
- The meshes remain insufficient 3D for the elements of order 1: stresses and strains of the modelizations A, C, E and L (especially for the modelization L in PYRAM5).
- The pyramids 3D give results similar to the other elements, with equivalent mesh.

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- The modelizations N and P with basic effect and pressure constant or variables give of good results.