

SHLL100 - Harmonic response of a bar per dynamic substructuring

Abstract:

The scope of application of this test relates to the dynamics of structures, and more particularly the harmonic computation of response per dynamic substructuring.

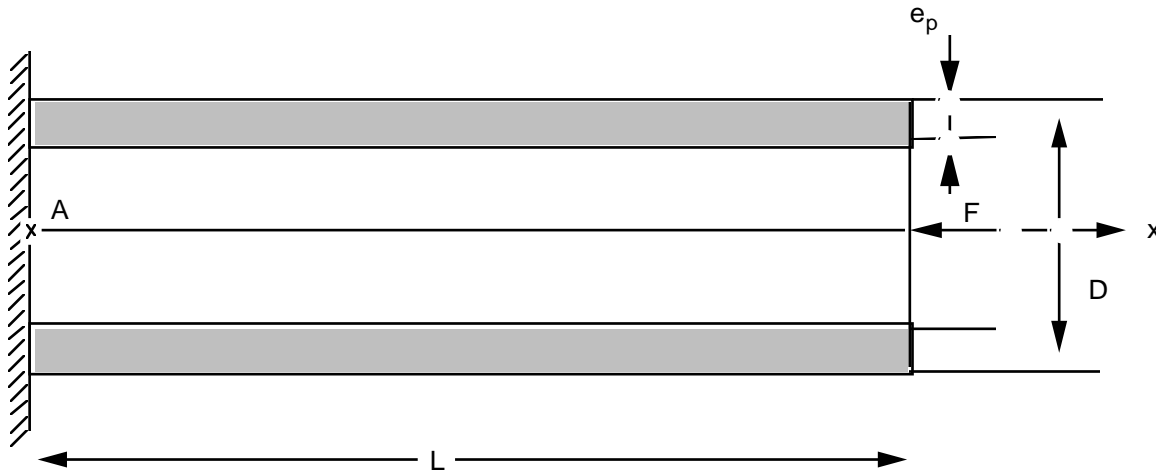
It is a question of calculating the harmonic response in traction and compression of a clamped beam - free modelled by elements of the type "bars". The modelled structure is damped (damping of Rayleigh by elements).

The results of reference result from a direct harmonic computation. This test thus makes it possible to validate the computational tools of harmonic response per substructuring established in *Code_Aster* and more particularly:

- the catch in depreciation account by element,
- the computation of the second member including the harmonic loading,
- the restitution of the harmonic response on a mesh squelette, including the fields of displacement, velocity and acceleration.

1 Problem of reference

1.1 Geometry



$$L = 1 \text{ m}$$

$$D = 0,2 \text{ m} - \text{Section circular}$$

1.2 Material properties

$$E = 1.10^{10} \text{ Pa}$$

$$\nu = 0.3$$

$$\rho = 1.10^4 \text{ kg/m}^3$$

Damping of Rayleigh per element: $\alpha_e = 0.1$ $\beta_e = 0.1$

1.3 Boundary conditions and loadings

Fixed support in the end A : $u(0) = n(0) = w(0) = 0$.

For all point: $M(x)$ $n(0) = w(0) = 0$.

Harmonic loading in time, at the loose lead:

- directional sense: according to x ,
- amplitude: 100 N ,
- frequency: 100 Hz .

1.4 Initial conditions

Without object for a harmonic computation of response.

2 Reference solution

2.1 Method of calculating used for the reference solution

There exists an analytical solution detailed in the reference [bib2].

Let us use the following notations:

E	:	Young's modulus
L	:	length of the bar
A	:	section of the bar
N	:	normal force directed according to the axis X
α, β	:	damping coefficients of Rayleigh
Ω	:	excitation frequency

and let us pose

$$r = \sqrt{\frac{1 + \beta^2 / \Omega^2}{1 + \alpha^2 / \Omega^2}}$$

$$k = p + iq = \Omega \sqrt{\frac{p}{2E}} \left[\sqrt{r - \frac{1 - \alpha\beta}{1 + \alpha^2 \Omega^2}} + i \sqrt{r + \frac{1 - \alpha\beta}{1 + \alpha^2 \Omega^2}} \right]$$

displacement in an unspecified $M(x)$ point is given by:

$$V(x) = \frac{N}{EA} \frac{A}{(p+iq)(1+i\Omega\alpha)} \frac{sh\ px \cos qx + i ch\ px \sin qx}{ch\ L \cos qL + i sh\ pL \sin qL}$$

	Displacement (m)	Velocity (m/s)	real (m/s ²)
Acceleration Left	- 7.00 10-11	- 3.18 10-6	2.76 10-5
imaginary Part	5.07 10-9	- 4.40 10-8	- 2.00 10-3

2.2 Results of reference

Fields of displacement, velocity and acceleration of the loose lead of the bar.

2.3 Uncertainty on the numerical

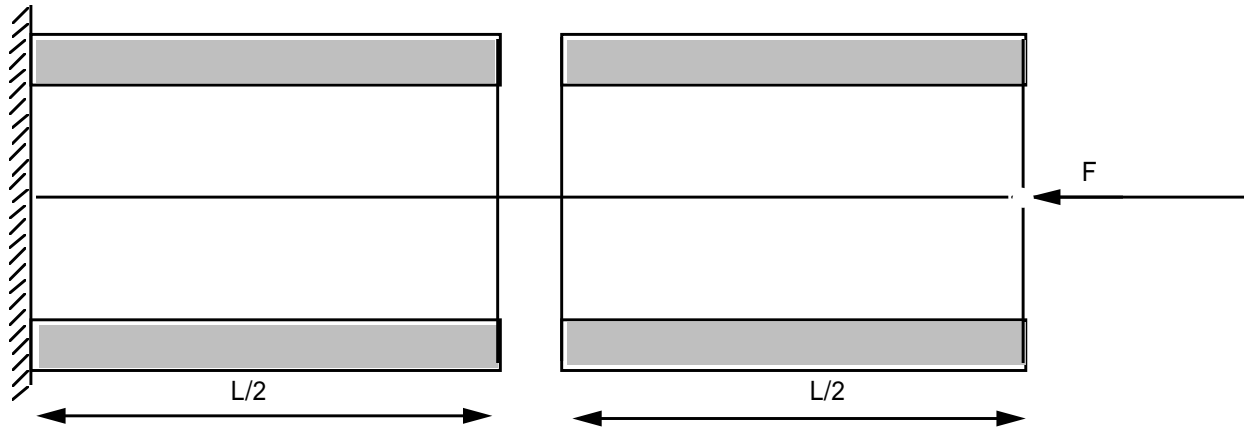
solution Solution.

2.4 Bibliographical references

- 1) T. KERBER "harmonic Substructuring in *the Code_Aster*", Ratio EDF, HP - 61/93 - 104.
- 2) G. ROBERT, analytical Solutions in dynamics of structures, Ratio Samtech n°121, March 1996.
- 3) P. RICHARD, Methods of substructuring in *the Code_Aster*, Ratio interns EDF - DER, HP-61/92-149.

3 Modelization A

3.1 Characteristic of the modelization



the bar is cut out in 2 parts of equal size. Each substructure considered is with a grid in segments to which elements are affected "bars".

The structure is studied using the method of the harmonic substructuring with interfaces of the HARMONIC type CRAIG-BAMPTON.

Modal base used is made up of 4 eigen modes for substructure of right, of 5 eigen modes for substructure of left to which the harmonic constrained modes associated are added with the interfaces (calculated with 300 Hz . This value of the pulsation does not have any influence on result, it is arbitrary [bib3]).

3.2 Characteristics of the mesh

Many nodes: 5

Number of meshes and types: 5 SEG2

3.3 Quantities tested and results

Displacement (m)				
	Reference	Aster	% difference	real
Tolerance Left	$-7.00 \cdot 10^{-11}$	$-7.00 \cdot 10^{-11}$	-0.007	$2 \cdot 10^{-3}$
imaginary Part	$5.07 \cdot 10^{-9}$	$5.07 \cdot 10^{-9}$	-0.097	$2 \cdot 10^{-3}$
real (m/s)				
Velocity Left	$-3.18 \cdot 10^{-6}$	$-3.18 \cdot 10^{-6}$	-0.078	$2 \cdot 10^{-3}$
imaginary Part	$-4.40 \cdot 10^{-8}$	$-4.40 \cdot 10^{-8}$	0.033	$2 \cdot 10^{-3}$
real (m/s^2)				
Acceleration Left	$2.76 \cdot 10^{-5}$	$2.76 \cdot 10^{-5}$	0.133	$2 \cdot 10^{-3}$
imaginary Part	$-2.00 \cdot 10^{-3}$	$-2.00 \cdot 10^{-3}$	-0.019	$2 \cdot 10^{-3}$

4 Summary of the results

the accuracy on the complex coordinates the fields of displacement velocity and acceleration is lower than 0,1% .

This test thus validates the operators of harmonic substructuring.