

## SDLS113 – Plate in plane strain under harmonic pressure

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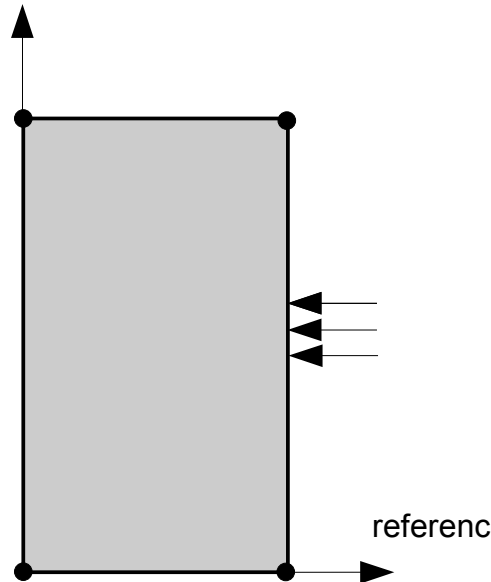
### Abstract:

The purpose of this benchmark is to validate the computation of a plate in plane strain (`D_PLAN`) subjected to a sinusoidal pressure using a harmonic computation.

For that, one carries out two computations on the same model, a harmonic computation and a transient computation. The computation transitory is used as reference.

## 1 Problem of XYABDCpGéométrie

### 1.1



Coordinated of the points expressed in meters:

$$A : (0.0, 0.0)$$

$$B : (0.35, 0.0)$$

$$C : (0.35, 0.6)$$

$$D : (0.0, 0.6)$$

### 1.2 Elastic properties of the material

- $E = 1.8 \times 10^{11} Pa$  Modulus Young
- $\nu = 0.3$  Poisson's ratio
- $\rho = 7800.0 kg.m^{-3}$  Density
- $\alpha = 3 \times 10^{-5} s$
- $\beta = 0.001 s^{-1}$

the coefficients  $\alpha$  and  $\beta$  make it possible to build a viscous damping matrix proportional to the stiffness and the mass  $[C] = \alpha [K] + \beta [M]$  .

### 1.3 Boundary conditions and loadings

- Fixed support on the side  $AD$   
 $DX = 0.0 m$  ,  $DY = 0.0 m$
- on the east side  $BC$  subjected to a harmonic pressure of amplitude  $p = 10^5 Pa$  to a frequency  $f = 1500 Hz$

## 2 Reference solution

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### 2.1 Method of calculating

It is a question of calculating the response of a plate subjected to a harmonic pressure on a side of the plate and embedded on the opposite side.

The reference solution is obtained by carrying out a computation of transient response with operator `DYNA_VIBRA` by means of the diagram of integration of Newmark with the parameters  $\alpha = 0.25$  and  $\delta = 0.5$ .

### 2.2 Quantities and results of reference

One proposes to test the following quantities:

- Displacement following  $x$  to the point of coordinates  $(0.0816, 0.165)$
- Forced and strain to the Gauss point of a mesh containing the node of coordinates  $(0.3383, 0.39)$
- Forced and strain to the node of coordinates  $(0.3383, 0.39)$

### 2.3 Uncertainties on the solution

One considers that the mode is established at the end of 90 periods. The values of reference selected are those raised on 98<sup>ième</sup> and the 99<sup>ième</sup> periods of the transient response.

## 3 Modelization A

### 3.1 Characteristic of the modelization A

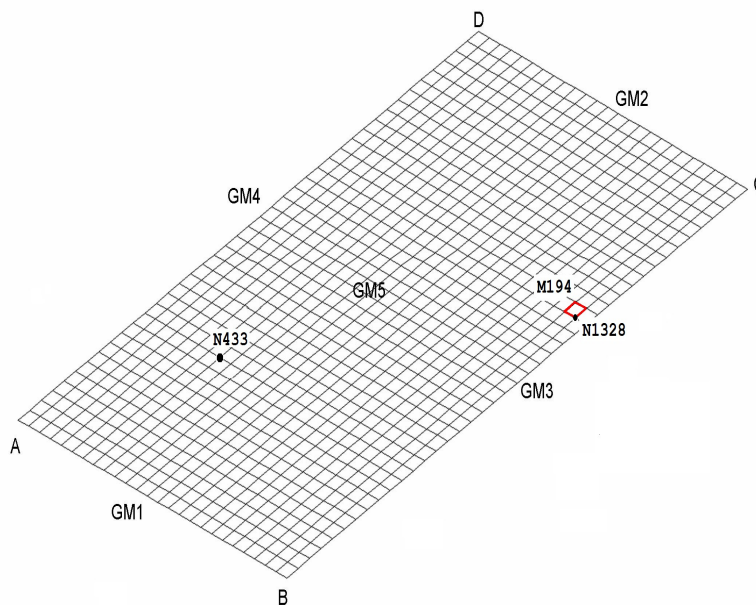
Modelization D\_PLAN

### 3.2 Characteristics of the mesh

Many nodes: 1271  
Number of meshes:  
SEG2 : 140  
QUAD4 : 1200

Mesh group:

GM1 : dimensioned AB  
GM2 : dimensioned CD  
GM3 : dimensioned BC  
GM4 : dimensioned AD  
GM5 : face ABCD



N433 : (0.0816, 0.165)

N1328 : (0.3383, 0.39)

## 3.3 Quantities tested and results

Identification	Reference
DX to the node N433	$3.9896 E - 8 m$
SIXX at the Gauss point number 1 of the mesh M194	$98461 Pa$
SIXX with the node N1328 of the mesh M194	$98100 Pa$
EPXX at the Gauss point number 1 of the mesh M194	$5.2747 E - 7$
EPXX with the node N1328 of the mesh M194	$5.2772 E - 7$

One calculates kinetic energy ECIN\_ELEM of the mesh M194 :

Component	option	Reference (NON_REGRESSION)	Aster	tolerance
<b>harmonic Computation</b>				
ECIN_ELEM	TOTAL	1.91599 10-6	1.9159851 10-6	0.1%
<b>Transient computation</b>				
ECIN_ELEM	TOTAL	1.78915 10-6	1.7891507 10-6	0.1%

## 4 Summary of the results

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the computation results of the harmonic response are very close to those obtained with an equivalent transient computation which was used as reference.