
SDLL01 - Short beam on simple bearings

Abstract:

This two-dimensional problem consists in searching the frequencies of vibration of a mechanical structure made up of a beam out of simple bearings at its two ends. This case test of Structural mechanics corresponds to a dynamic analysis of a linear model having a linear behavior. One compared to the studies the influence of the position of the points considered as fulcrums (points on neutral fiber or points offset at the base of the beam) neutral fiber of a thick beam.

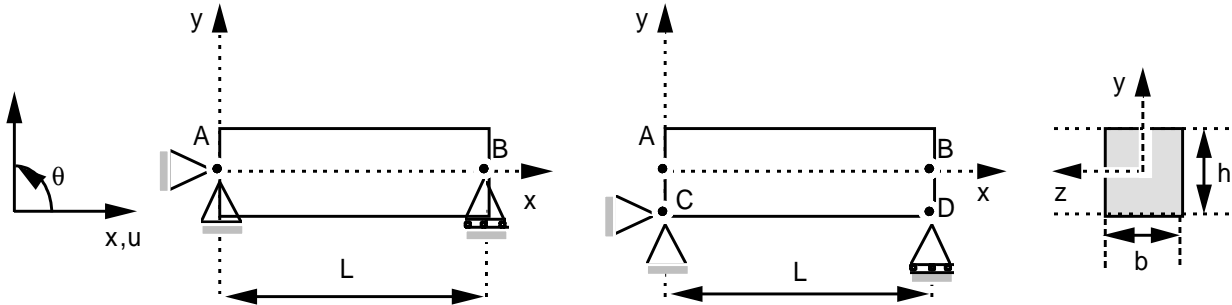
This test makes it possible to test part of the features which relate to the beams of Timoshenko, rigid connections and the search for eigenfrequencies by inverse iterations.

The results got with the fulcrums on neutral fiber, is with the offset fulcrums are compared with analytical computations on the beams of Timoshenko. The results got with the offset fulcrums are compared with results of NON-regression.

When the fulcrums are offset, one observes a coupling between the various modes of tension - compression and bending.

1 Problem of reference

1.1 rectangular



Geometry Cross-section:

| | |
|----------|---------------------------|
| height: | $h=0.2\text{ m}$ |
| width: | $b=0.1\text{ m}$ |
| area: | $A=2.10^{-2}\text{ m}^2$ |
| inertia: | $I_z=6.667\ 10^{-5}$ |
| shears: | $A_y=A_z=1.17692$ |
| torsion: | $J_x=0.45776042\ 10^{-4}$ |

Length of the beam

$$L=1.\text{ m}$$

Coordinated of the points (m) :

| | A | B | C | D |
|---|----|----|------|------|
| x | 0. | 1. | 0. | 1. |
| y | 0. | 0. | -0.1 | -0.1 |

1.2 Material properties

$$E=2.10^{11}\text{ Pa}$$

$$\nu=0.3$$

$$\rho=7800.\text{ kg/m}^3$$

1.3 Boundary conditions and loadings

| | | | | |
|------------|-------|----------|-------|--------|
| Problem 1: | Not A | $u=v=0.$ | Not B | $v=0.$ |
| Problem 2: | Not C | $u=v=0.$ | Not D | $v=0.$ |

2 Reference solution

2.1 Method of calculating used for the reference solution

the reference solution is that given in the book of Timoshenko on the theory of vibrations of the beams and plates ([1]):

Problem 1: Analytical computation

the equation of bending of the nonslender beams gives the formulation of Timoshenko, by superimposing the effects of the pure bending, the shear deformations and the inertia of rotation.

The eigenfrequencies in traction and compression are given according to this theory by:

$$f_i = \frac{\lambda_i}{2\pi L} \sqrt{\frac{E}{\rho}} \text{ with } \lambda_i = \frac{(2i-1)}{2} \pi \quad i=1,2,\dots$$

One finds in the reference [1] an equivalent formula for the modes of bending.

Problem 2:

The problem not having an analytical solution, the solution is established by results of NON-regression.

The modes of bending and traction and compression are coupled.

2.2 Results of reference

Problem 1: the first 6 eigen modes.

Problem 2: the first 5 eigen modes.

2.3 Uncertainty on the solution

Problem 1: analytical solution. “

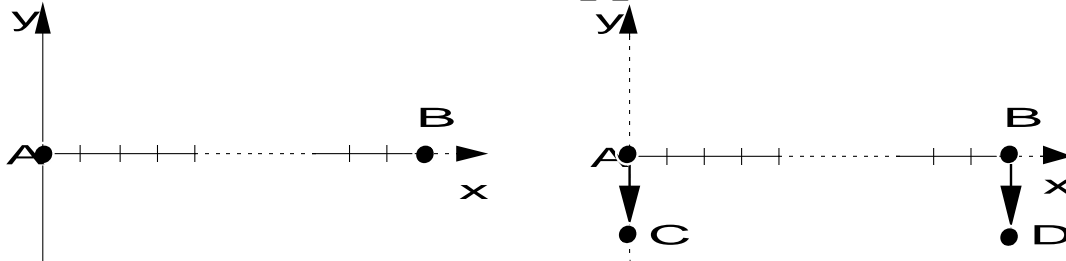
2.4 Bibliographical References

- [1] S.P. TIMOSHENKO, D.H. YOUNG, W. WEAVER. Vibrations Problems in Engineering. New - York: Wiley & Sons, 4^o edition, p. 415 (1974).

3 Modelization A

3.1 Characteristic of the modelization

One uses the beam element right of Timoshenko: POU_D_T



Problem 1:

Cutting: beam: AB 40 meshes limiting

SEG2 Conditions:

in all the nodes

in A :

in B :

```
DDL_IMPO = (GROUP_NO = "AB", DZ=0., DRX=0, DRY=0.)
            (NOEUD=' A', DX=0., D=0. )
            (NOEUD=' B', DY=0. )
```

Problem 2:

Cutting: beam: AB 40 meshes rigid

SEG2 2 elements AC BC : 2 meshes limiting

SEG2 Conditions:

in all the nodes

in C :

in D :

```
DDL_IMPO = (TOUT=' OUI', DZ=0., DRX=0, DRY=0.)
            (NOEUD=' IT, DX=0., DY=0. )
            (NOEUD=' OF, DY=0. )
```

Names of the nodes:

Not A = $N100$

Not C = $N300$

Not B = $N200$

Not D = $N400$

3.2 Characteristic of the mesh

Many nodes: 43

Number of meshes and types: 42 SEG2

3.3 Remarks

Definition of the rigid beams AC and BD :

Section: $H_y=0.2$ $H_z=0.2$.

Material: $E=2.10^{16}$ $\rho=0$.

3.4 Quantities tested and Frequency

results (Hz)

| Eigen mode | Reference | Aster | tolerance |
|------------------|-----------|-----------|-----------|
| Problem 1 | | | |
| bending 1 | 431.555 | 431.8916 | 0.2% |
| tension 1 | 1265.924 | 1266.0056 | 0.2% |
| bending 2 | 1498.295 | 1500.7635 | 0.2% |
| bending 3 | 2870.661 | 2873.5344 | 0.2% |
| tension 2 | 3797.773 | 3799.9692 | 0.2% |
| bending 4 | 4377.837 | 4370.8206 | 0.2% |

| Eigen mode | Reference | Aster | tolerance |
|------------------|-----------|-----------|-----------|
| Problem 2 | | | |
| 1 | 392.8 | 394.4774 | 0.5% |
| coupling 2 | 922.2 | 922.6072 | 0.1% |
| bending 3 | 1592.0 | 1638.2311 | 3% |
| tension 4 | 2629.2 | 2778.7000 | 5.8% |
| compression 5 | 3126.2 | 3261.6699 | 4.5% |

One calculates the kinetic energy of the first beam element connected to the point A of problem 1:

| Component | option | Reference (NON_REGRESSION) | Aster | % TOTAL |
|------------|-----------|-------------------------------|-----------|---------|
| difference | ECIN_ELEM | 51366.0 | 51366.027 | 1% |

3.5 Remarks

Computations carried out by:

Problem 1:

MODE_ITER_INV OPTION=' AJUSTE ' LIST_FREQ= (430. , 4500.)

Problem 2:

MODE_ITER_INV OPTION=' AJUSTE ' LIST_FREQ= (380. , 3300.)

Contents of the file results:

Problem 1:

the first 6 eigenfrequencies, modal eigenvectors and parameters.

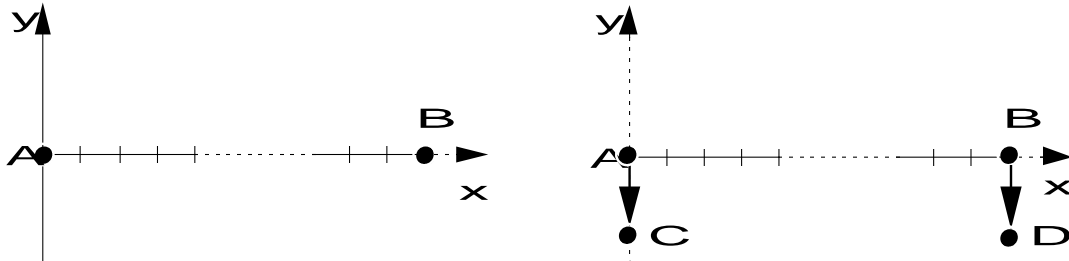
Problem 1:

the first 5 eigenfrequencies, modal eigenvectors and parameters.

4 Modelization B

4.1 Characteristic of modelization

POU_D_TG



Problem 1:

Cutting: beam: *AB* 40 meshes limiting
 SEG2 Conditions:
 in all the nodes DDL_IMPO = (GROUP_NO=' AB', DZ=0., DRX=0, DRY=0.)
 in *A* : (GROUP_NO=' A' DX=0., DY=0.)
 in *B* : (GROUP_NO=' B', DY=0.)

Problem 2:

Cutting: beam *AB*: 40 meshes rigid
 SEG2 2 elements *AC BD* : 2 meshes limiting
 SEG2 Conditions:
 in all the nodes DDL_IMPO = (TOUT=' OUI', DZ=0., DRX=0, DRY=0.)
 in *C* : (GROUP_NO=' IT, DX=0., DY=0.)
 in *D* : (GROUP_NO=' OF, DY=0.)
 Names of the nodes: Not *A* = *N100* Not *C* = *N300*
 Not *B* = *N200* Not *D* = *N400*

4.2 Characteristic of the mesh

Many nodes: 43
 Number of meshes and types: 42 SEG2

4.3 Remarks

Definition of the rigid beams *AC* and *BD* :

Section: $H_y=0.2$ $H_z=0.2$.

Material: $E=2.10^{16}$ $\rho=0$.

4.4 Quantities tested and Frequency

results (Hz)

| Eigen mode | Reference | Aster | tolerance | |
|------------------|-----------|-----------|-----------|------|
| Problem 1 | | | | |
| bending 1 | 431.555 | 431.8916 | 0.2% | |
| tension 1 | 1265.924 | 1266.0056 | 0.2% | |
| bending 2 | 1498.295 | 1500.7635 | 0.2% | |
| bending 3 | 2870.661 | 2873.5344 | 0.2% | |
| tension 2 | 3797.773 | 3799.9692 | 0.2% | |
| bending 4 | 4377.837 | 4370.8206 | 0.2% | |
| Problem 2 | | | | |
| 1 | 392.8 | ± 2.7% | 394.4774 | 0.5% |
| coupling 2 | 922.2 | ± 5.7% | 922.6072 | 0.1% |
| bending 3 | 1592.0 | ± 2.9% | 1638.2311 | 3% |
| tension 4 | 2629.2 | ± 5.7% | 2778.7000 | 5.8% |
| compression 5 | 3126.2 | ± 4.3% | 3261.6699 | 4.5% |

4.5 Remarks

Computations carried out by:

Problem 1:

ITERATIONS_INVERSESOPTION : LIST_FREQ "ADJUSTS": (430. , 4500.)

Problem 2:

ITERATIONS_INVERSESOPTION : LIST_FREQ "ADJUSTS": (380. , 3300.)

Contents of the file results:

Problem 1:

the first 6 eigenfrequencies, modal eigenvectors and parameters.

Problem 1:

the first 5 eigenfrequencies, modal eigenvectors and parameters.

5 Summary of the

results the problem without eccentricity is correctly treated. That with eccentricity is validated only by NON-regression.