

---

## GCPC002 - Prismatic test-tube fissured in 3D

---

### Summarized:

This case test of elastic design is resulting from an industrial problem. It makes it possible to qualify the solver PCG with various preconditioners.

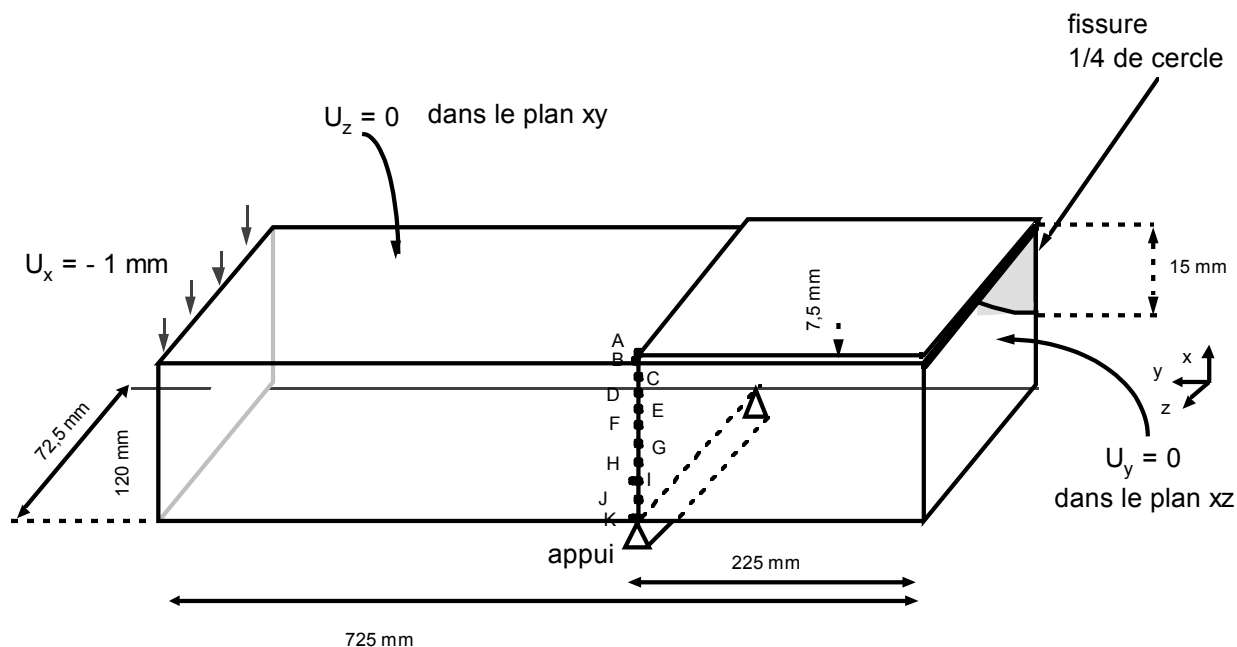
The values of reference result from a computation carried out on the mesh with code PERMAS.

The test comprises 3 modelizations on the same problem of reference: modelization 3D of a prismatic quarter of test-tube fissured in 4784 pentahedrons with 15 nodes and 598 hexahedrons with 20 nodes, are 16565 nodes.

In the previous models, this case test was named SSLV103 and YYYY104.

## 1 Problem of reference

### 1.1 Geometry



Cote en x : (mm)	A : 127.5	D : 105.00	G : 60.00	J : 15.00
	B : 123.75	E : 90.00	H : 45.00	K : 0.00
	C : 120.00	F : 75.00	I : 30.00	

### 1.2 Material properties

$$E = 210000 \text{ MPa}$$

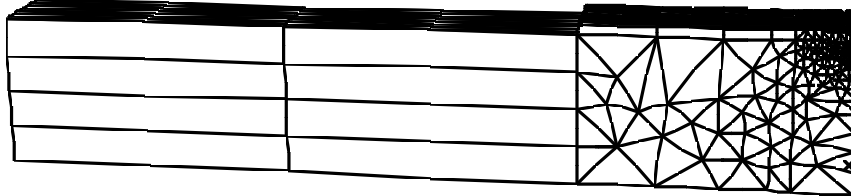
$$\nu = 0.3$$

### 1.3 Boundary conditions and loadings

$U_z = 0$	in the plane:	$Z = 0$	
$U_x = 0$	on the segment:	$X = 0$	$Y = 225$
$U_y = 0$	in the plane:	$Y = 0$	out of crack
$U_x = -1$	on the segment:	$X = 120$	$Y = 725$

## 2 Modelization of reference

### 2.1 Modelization common to all the tests



A	⇒	NO13943	G	⇒	NO15862
B	⇒	NO13944	H	⇒	NO15863
C	⇒	NO15854	I	⇒	NO15868
D	⇒	NO15855	J	⇒	NO15869
E	⇒	NO15858	K	⇒	NO15866
F	⇒	NO15860			

#### 2.1.1 Mesh

Many nodes: 16565

Number of meshes and types: 598 HEXA20 , 4784 PENTA15.

#### 2.1.2 Boundary conditions

in all the nodes of the plane  $Y=0$  except crack

(GROUP\_NO=' Supy', DY=0.)

in all the nodes of segment  $X=0$   $Y=225$

(GROUP\_NO=' Appui', DX=0.)

in all the nodes of plane  $Z=0$

(GROUP\_NO=' Supz', DZ=0.)

in all the nodes of segment  $X=120$   $Y=725$

(GROUP\_NO=' Charge', DX=-1.)

## 3 Reference solution

### 3.1 Method of calculating used for the reference solution

the reference solution is that obtained on the same mesh with code PERMAS (Version 3.12), computations carried out in 1997.

### 3.2 Result of reference: values tested

Identification	Reference	Tolerance (%)
A DX	0.31725E-02	1.E-3
A DY	0.28244E-01	1.E-3
A DZ	- 0.29278E-02	1.E-3
B DX	0.38304E-02	1.E-3
B DY	- 0.31279E-02	1.E-3
B DZ	0.48316E-03	1.E-3
C DX	0.00000E+00	1.E-3
C DY	- 0.67226E-01	1.E-3
C DZ	0.58204E-02	1.E-3

Warning : The translation process used on this website is a "Machine Translation". It may be imprecise and inaccurate in whole or in part and is provided as a convenience.

## 4 Modelization A

---

### 4.1 Characteristic of the modelization

The modelization is characterized by the choices of imposition of boundary conditions and the sequence of the commands of following resolution.

#### Commands

NUME DDL	METHODE	"PCG"
	RENUM	"SANS"
TO FACTORIZE	PRE COND	"LDLT INC"
TO SOLVE		
TO FACTORIZE	PRE COND	"LDLT SP"
TO SOLVE		

## 5 Modelization B

---

### 5.1 Characteristic of the modelization

The modelization is characterized by the choices of imposition of boundary conditions and the sequence of the commands of following resolution.

#### Commands

NUME DDL	METHODE	"PCG"
	RENUM	"RCMK"
TO FACTORIZE	PRE COND	"LDLT INC"
TO SOLVE		
TO FACTORIZE	PRE COND	"LDLT SP"
TO SOLVE		

## 6 Modelization C

---

### 6.1 Characteristic of the modelization

The modelization is characterized by the choices of imposition of boundary conditions and the sequence of the commands of following resolution.

#### Commands

MECA STATIQUE	solver	METHODE	"PCG"
		RENUM	"SANS"
		PRE COND	"LDLT INC"
MECA STATIQUE	solver	METHODE	"PCG"
		RENUM	"SANS"
		PRE COND	"LDLT SP"

## 7 Summary of the results

---

the various approaches of resolution make it possible to obtain the same accuracy of the results.